



CONSULTING

PLANNING ■ DESIGN ■ CONSTRUCTION

MEREDITH PROPERTY

**City of Ontario
San Bernardino County, California**

CONCEPTUAL HYDROLOGY REPORT

Prepared For:

SARES REGIS GROUP
18802 Bardeen Avenue
Irvine, California 92612-1521
(949)756-5959

Consultant:

RBF CONSULTING
14725 Alton Parkway
Irvine, California 92618
Contact: Thomas C. Carmody, P.E.
Rick L. Howe, P.E.
(949) 472-3493

April, 2014
JN 130346

Introduction

The purpose of this report is to conceptually show existing and proposed hydrologic conditions for the 257 acre Meredith Property Project. The project is in the City of Ontario, California and bounded by Vineyard Ave on the west, 4th St on the north, Interstate Freeway 10 on the south, and Archibald Ave on the east.

This report analyzes and quantifies the 100 year storm runoff rates in the existing and proposed condition for the site. Analysis was performed following the San Bernardino County Hydrology Manual (SBCHM) guidelines and utilized the Advanced Engineering Software (AES) to generate runoff rates (see backup in appendix). The site's drainage patterns, runoff rates, and storm drain infrastructure are shown in the two hydrology maps (see Existing and Proposed Hydrology Maps in appendix). Water Quality and incremental increase of Storm Runoff are addressed in the Specific Plan narrative for this project.

Existing Hydrology

The site shows signs that it has been tilled at some date in its' past, but is currently weed-laden open-space flat-land with gradients of 0.5% to 1.5%. Per the Existing Hydrology Map the southerly flowing Cucamonga Channel divides the site into parcel areas of 207 acres westerly (Watersheds 1, 2, & 3) and 50 acres easterly (Watersheds 4 & 5).

- Watershed 1: Runoff sheet flows south-easterly and is tributary to the Cucamonga Channel. A berm along the north side of Inland Empire prevents runoff from entering the roadway and forces the runoff easterly. All runoff flows over the channel wall into the channel.
- Watershed 2: Runoff from paved Inland Empire Blvd runs easterly into two catch basins just west of the Cucamonga Channel. The runoff enters a storm drain system that discharges to the channel.
- Watershed 3: Runoff sheet flows south-easterly and gathers along the north side of Interstate 10 then runs easterly. The runoff enters a drop inlet structure located in the Caltrans property just west of the Cucamonga Channel.
- Watershed 4: Runoff sheet flows south-westerly over the Cucamonga Channel wall into the channel.
- Watershed 5: Runoff north of Inland Empire flows south-easterly to a pipe running southerly under Inland Empire Blvd which discharges on the south side of the street. Inland Empire Blvd and the triangular parcel on the north-west corner of Inland Empire Blvd and Archibald Ave are tributary to two catch basins that discharge on the south side of the street. This concentrated flow is joined by sheet flow runoff from the parcel south of Inland Empire Blvd. The runoff migrates southerly to exit the site through an existing 42" pipe and headwall that lies within the Caltrans property.

Proposed Hydrology

The site is proposed to be mixed use of Commercial, Industrial, and Residential per the Specific Plan for this project. In all cases the site is expected to be considered to have a high percentage of impervious surfaces so it is assumed for calculations that Commercial Land use is used in the analysis. The proposed gradients are expected to be in the range between 0.5% and 1.5%. Per the Proposed Hydrology Map the site's drainage patterns and points of runoff discharge will be nearly the same as in the existing condition, but the site has been divided up into 6 watersheds.

- Watersheds 1, 2, and 3: Called PA-1 in the Specific Plan has a Land Use of Industrial. Runoff flows generally south-easterly across pavement or along local street-side curb and gutters. The runoff is expected to be collected in a water quality detention facility prior to discharge into a storm drain system tributary to the Cucamonga Channel.
- Watershed 4: Runoff from newly located paved Inland Empire Blvd will run easterly into two catch basins just west of the Cucamonga Channel. The runoff will enter a storm drain system that discharges to the channel.
- Watershed 5: Called PA-2 in the Specific Plan has a Land Use of Commercial. Runoff will flow generally easterly over the surface and within localized storm drain systems. The runoff is expected to be collected in a water quality detention facility prior to discharge into the existing storm drain system located in the Caltrans property just west of the Cucamonga Channel.
- Watershed 6: Called PA-3, PA-4, and PA-5 have Land Use of Urban Commercial and/or Urban Residential. The runoff from north of Inland Empire Blvd will be collected in a storm drain system to be conveyed southerly to the existing Caltrans outlet. The runoff from Inland Empire Blvd and the triangular parcel on the north-west corner of Inland Empire Blvd and Archibald Ave will be picked up in two catch basins within Inland Empire Blvd and conveyed southerly to the existing Caltrans outlet. The runoff from south of Inland Empire Blvd will also be conveyed to the Caltrans outlet. The runoff from all areas of this watershed is expected to be collected in water quality detention facilities prior to discharge.

Appendix:

EXISTING HYDROLOGY EXHIBIT

PROPOSED HYDROLOGY EXHIBIT

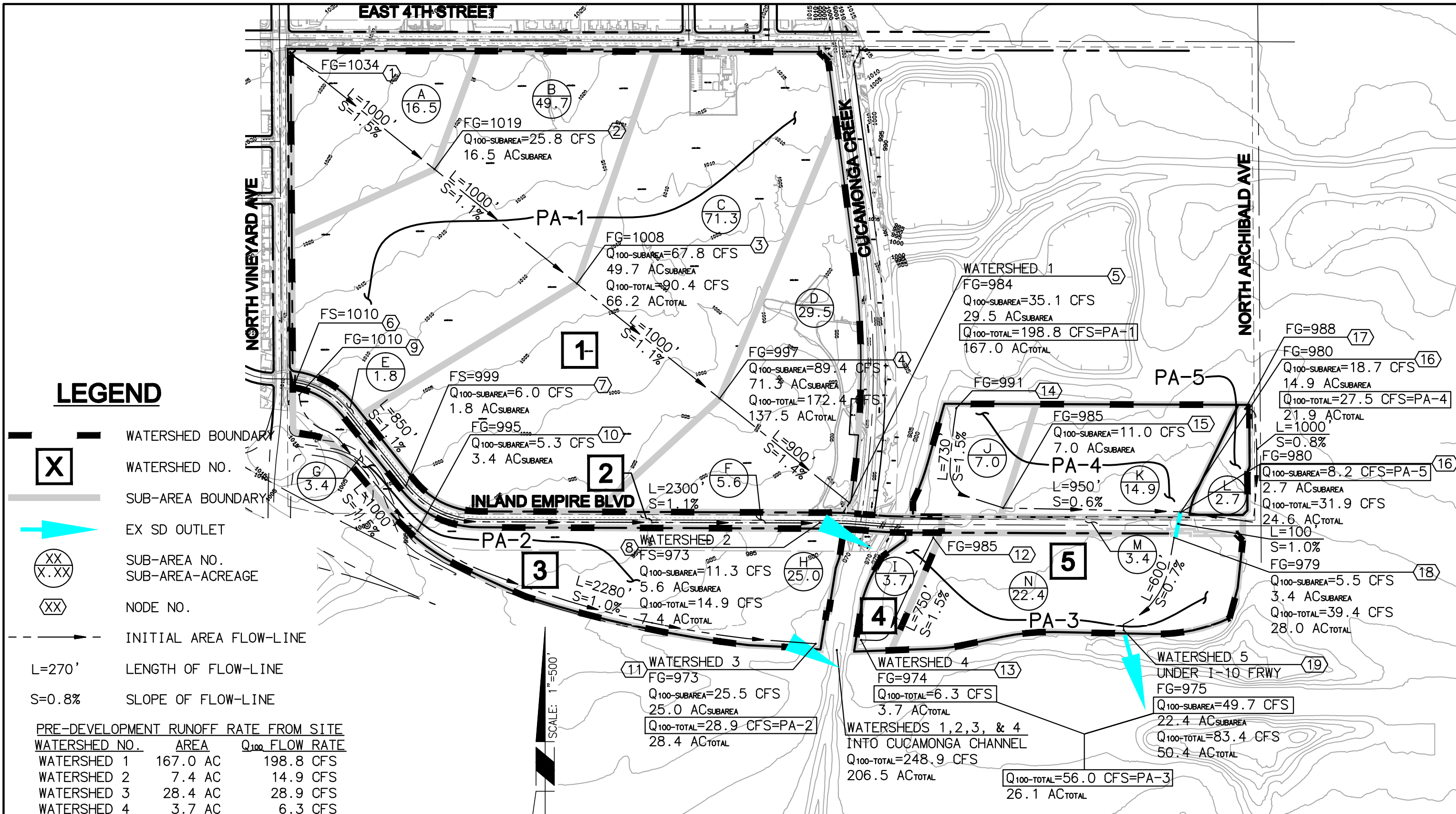
HYDROLOGY MANUAL ISOHYETALS AND RAINFALL BACK-UP INFORMATION

FIGURES: B1, B2, B3, B4, B5, B6, C13, AND D3

AES RATIONAL METHOD HYDROLOGY PROGRAM PRINTOUTS

EXISTING CONDITION: WATERSHEDS 1 THROUGH 5

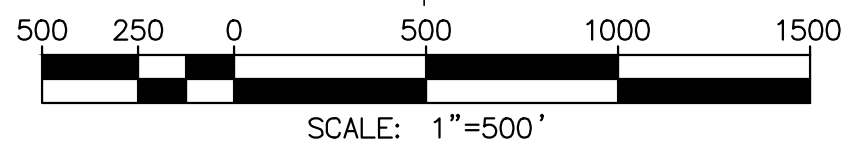
PROPOSED CONDITION: WATERSHEDS 1 THROUGH 6



LEGEND

- WATERSHED BOUNDARY
- WATERSHED NO.
- SUB-AREA BOUNDARY
- EX SD OUTLET
- SUB-AREA NO.
- SUB-AREA-ACREAGE
- NODE NO.
- INITIAL AREA FLOW-LINE
- $L=270'$ LENGTH OF FLOW-LINE
- $S=0.8\%$ SLOPE OF FLOW-LINE

PRE-DEVELOPMENT RUNOFF RATE FROM SITE		
WATERSHED NO.	AREA	Q ₁₀₀ FLOW RATE
WATERSHED 1	167.0 AC	198.8 CFS
WATERSHED 2	7.4 AC	14.9 CFS
WATERSHED 3	28.4 AC	28.9 CFS
WATERSHED 4	3.7 AC	6.3 CFS
WATERSHED 5	50.4 AC	83.4 CFS
TOTAL	256.9 AC	332.3 CFS



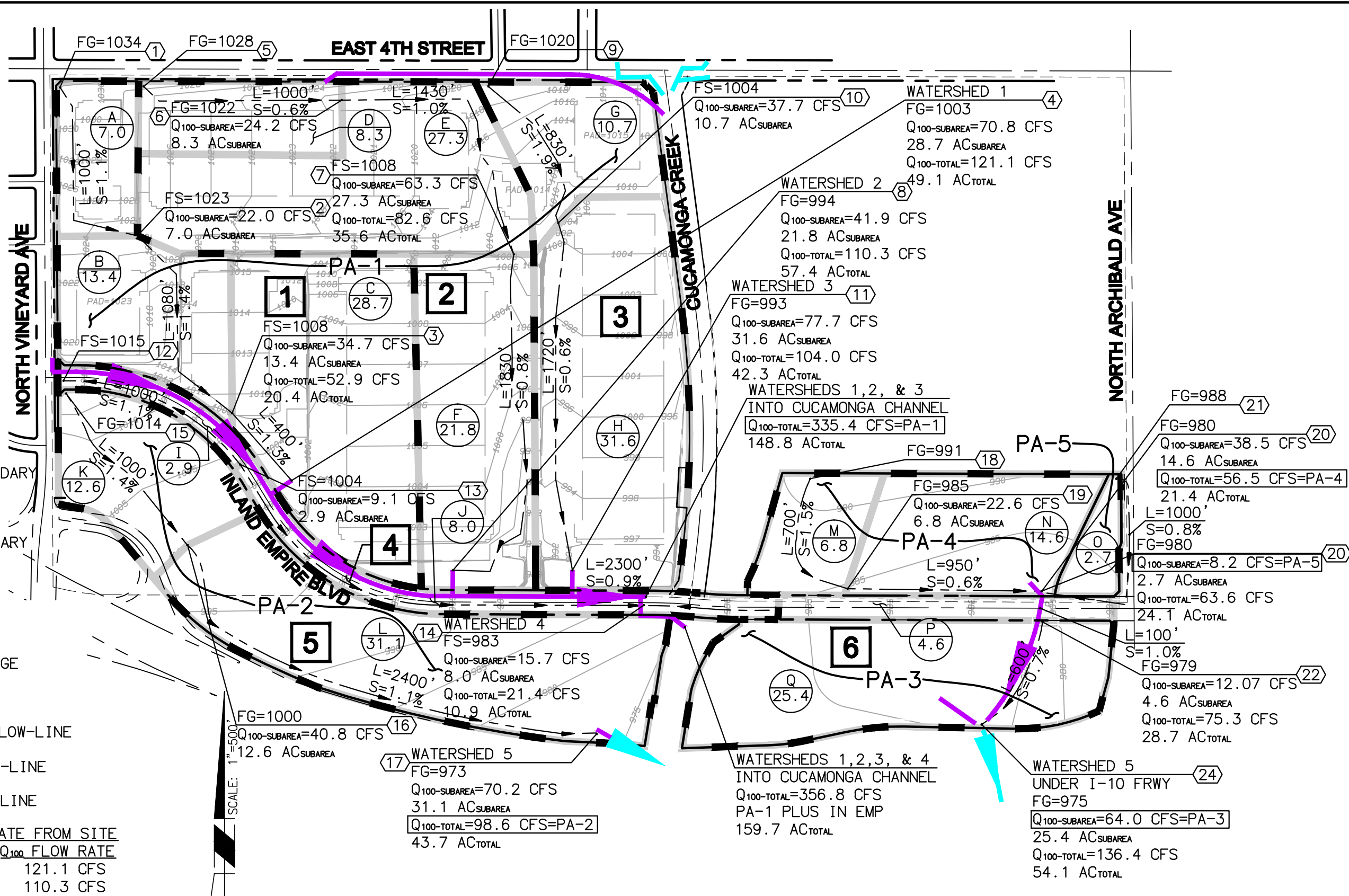
Prepared By:

PLANNING ■ DESIGN ■ CONSTRUCTION

14725 ALTON PARKWAY
IRVINE, CALIFORNIA 92618-2027
949.472.3505 ■ FAX 949.472.8122 ■ www.RBF.com

**SARES REGIS GROUP
MEREDITH PROPERTY
EXISTING HYDROLOGY
EXHIBIT**

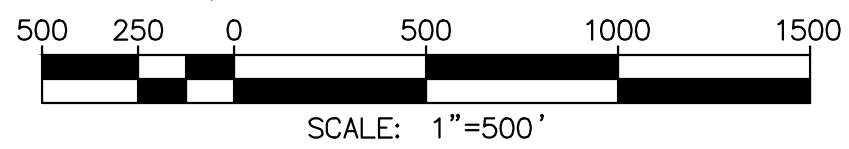
SCALE: 1" = 500' | DATE: 4/28/2014



LEGEND

- WATERSHED BOUNDARY
- WATERSHED NO.
- SUB-AREA BOUNDARY
- EX SD OUTLET
- PROP SD SYSTEM
- SUB-AREA NO.
SUB-AREA-ACREAGE
- NODE NO.
- INITIAL AREA FLOW-LINE
- $L=270'$ LENGTH OF FLOW-LINE
- $S=0.8\%$ SLOPE OF FLOW-LINE

POST-DEVELOPMENT RUNOFF RATE FROM SITE		
WATERSHED NO.	AREA	Q ₁₀₀ FLOW RATE
WATERSHED 1	49.1 AC	121.1 CFS
WATERSHED 2	57.4 AC	110.3 CFS
WATERSHED 3	42.3 AC	104.0 CFS
WATERSHED 4	10.9 AC	21.4 CFS
WATERSHED 5	43.7 AC	98.6 CFS
WATERSHED 6	54.1 AC	136.4 CFS
TOTAL	257.5 AC	591.8 CFS



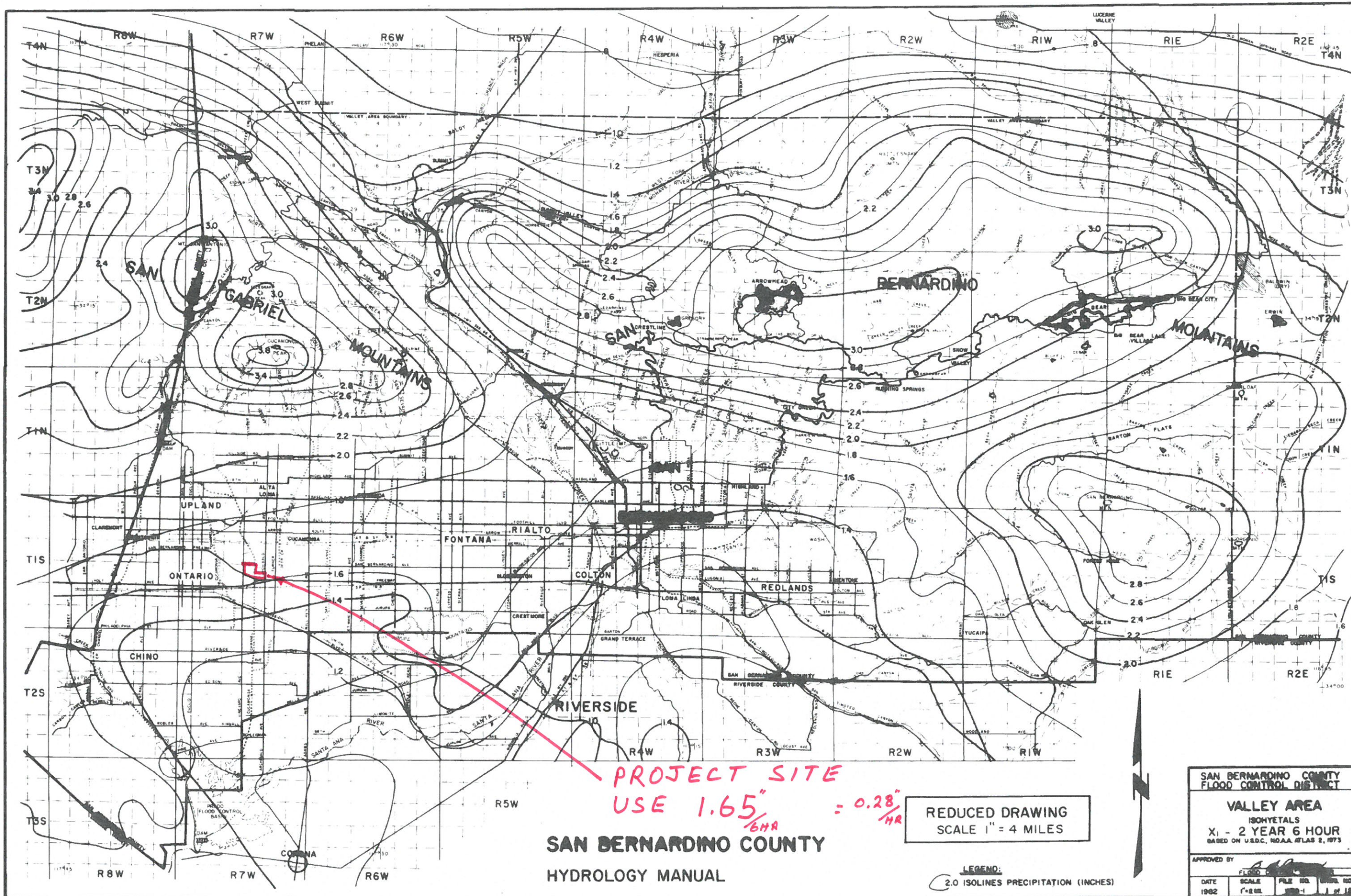
Prepared By:

PLANNING ■ DESIGN ■ CONSTRUCTION

14725 ALTON PARKWAY
IRVINE, CALIFORNIA 92618-2027
949.472.3505 ■ FAX 949.472.8122 ■ www.RBF.com

**SARES REGIS GROUP
MEREDITH PROPERTY
PROPOSED HYDROLOGY
EXHIBIT**

SCALE: 1" = 500' | DATE: 4/28/2014

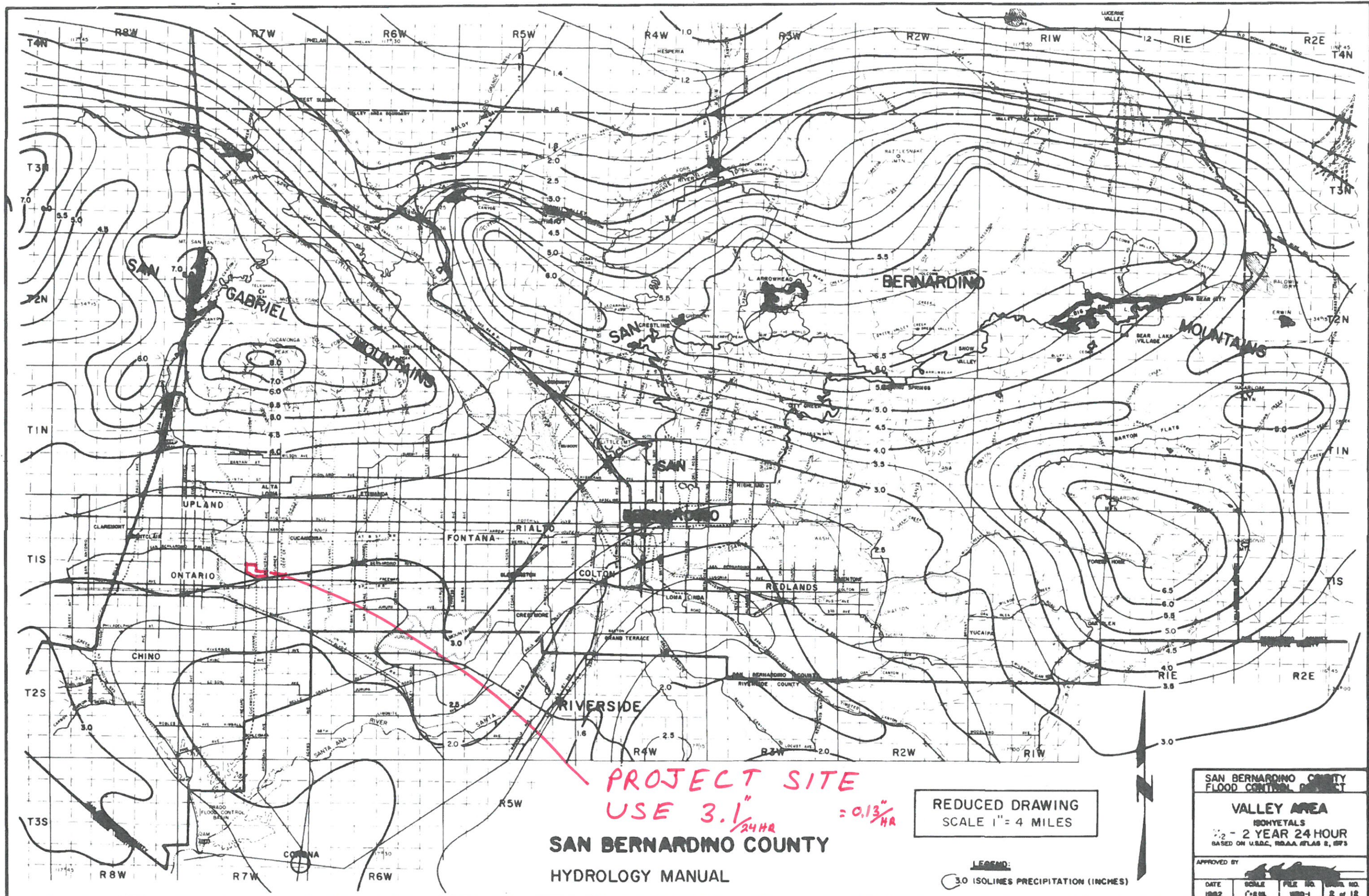


PROJECT SITE
 USE 1.65" $\frac{1}{6HR}$ = 0.28" $\frac{1}{HR}$
 SAN BERNARDINO COUNTY
 HYDROLOGY MANUAL

REDUCED DRAWING
 SCALE 1" = 4 MILES

LEGEND:
 2.0 ISOLINES PRECIPITATION (INCHES)

SAN BERNARDINO COUNTY FLOOD CONTROL DISTRICT			
VALLEY AREA ISOHYETALS X1 - 2 YEAR 6 HOUR BASED ON U.S.D.C. NOAA ATLAS 2, 1973			
APPROVED BY <i>[Signature]</i>			
DATE 1982	SCALE 1" = 4 MI.	FILE NO. 7-1	SHEET NO. 1 OF 12

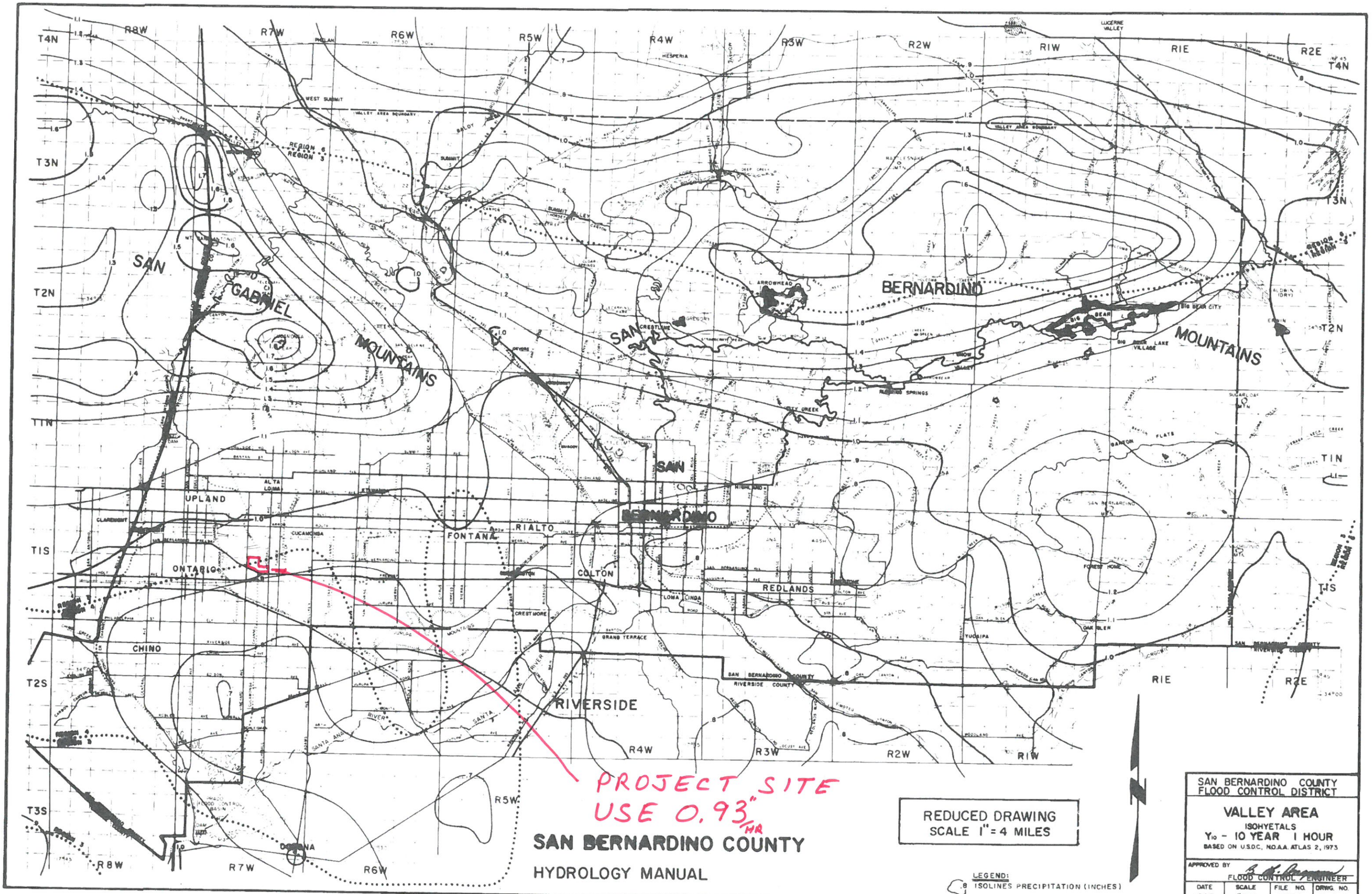


PROJECT SITE
 USE 3.1 ¹/_{24HR} = 0.13 ¹/_{HR}
 SAN BERNARDINO COUNTY
 HYDROLOGY MANUAL

REDUCED DRAWING
 SCALE 1" = 4 MILES

LEGEND:
 3.0 ISOLINES PRECIPITATION (INCHES)

SAN BERNARDINO COUNTY FLOOD CONTROL DISTRICT			
VALLEY AREA ISOHYETALS 2 - 2 YEAR 24 HOUR BASED ON U.S.D.C. NOAA ATLAS 2, 1973			
APPROVED BY:			
DATE 1982	SCALE 1" = 4 MI.	FILE NO. WB-1	SHEET NO. 8 of 12



*PROJECT SITE
USE 0.93" ^{HR}*

**SAN BERNARDINO COUNTY
HYDROLOGY MANUAL**

REDUCED DRAWING
SCALE 1" = 4 MILES

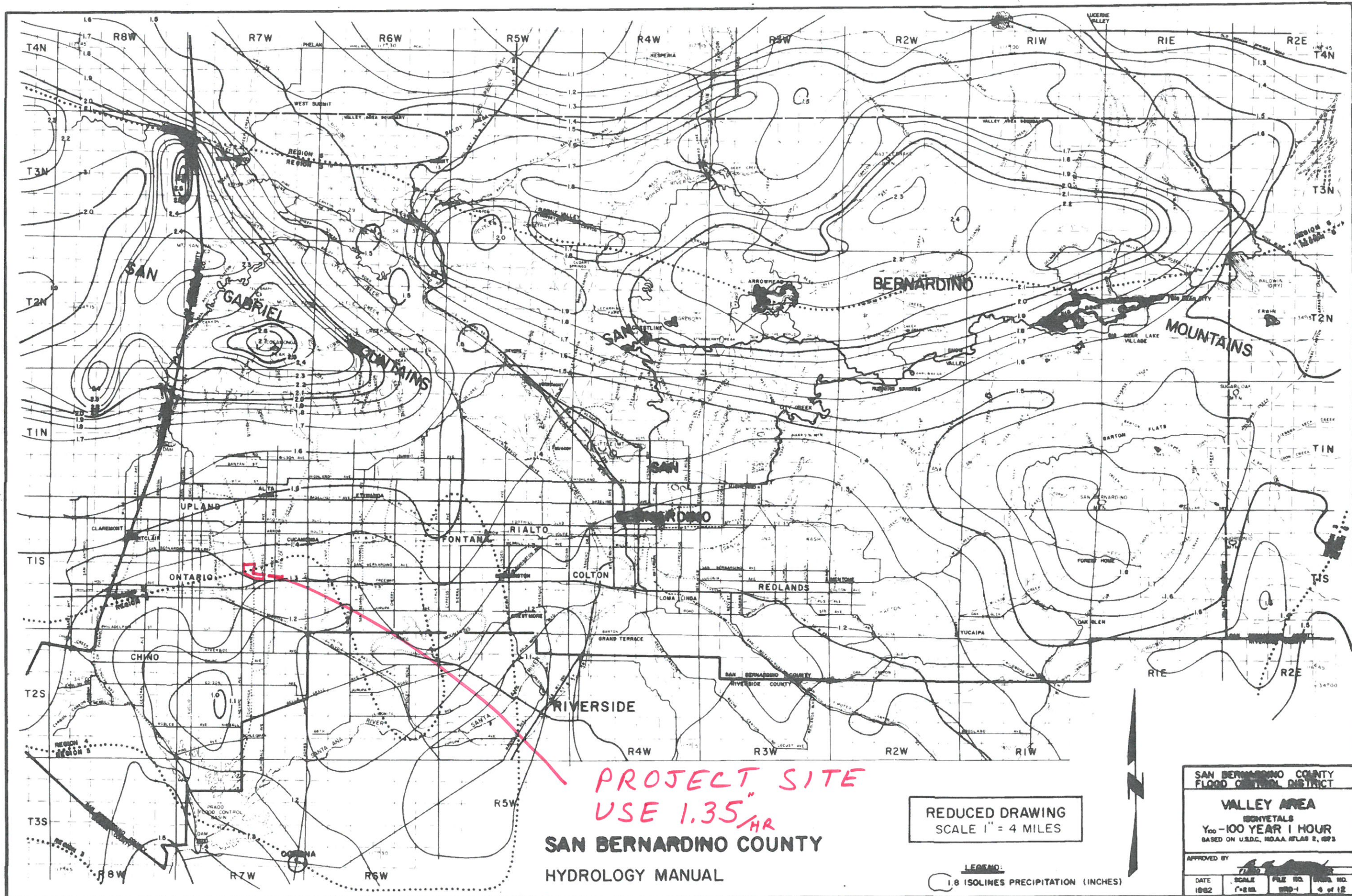
LEGEND:
ISOLINES PRECIPITATION (INCHES)

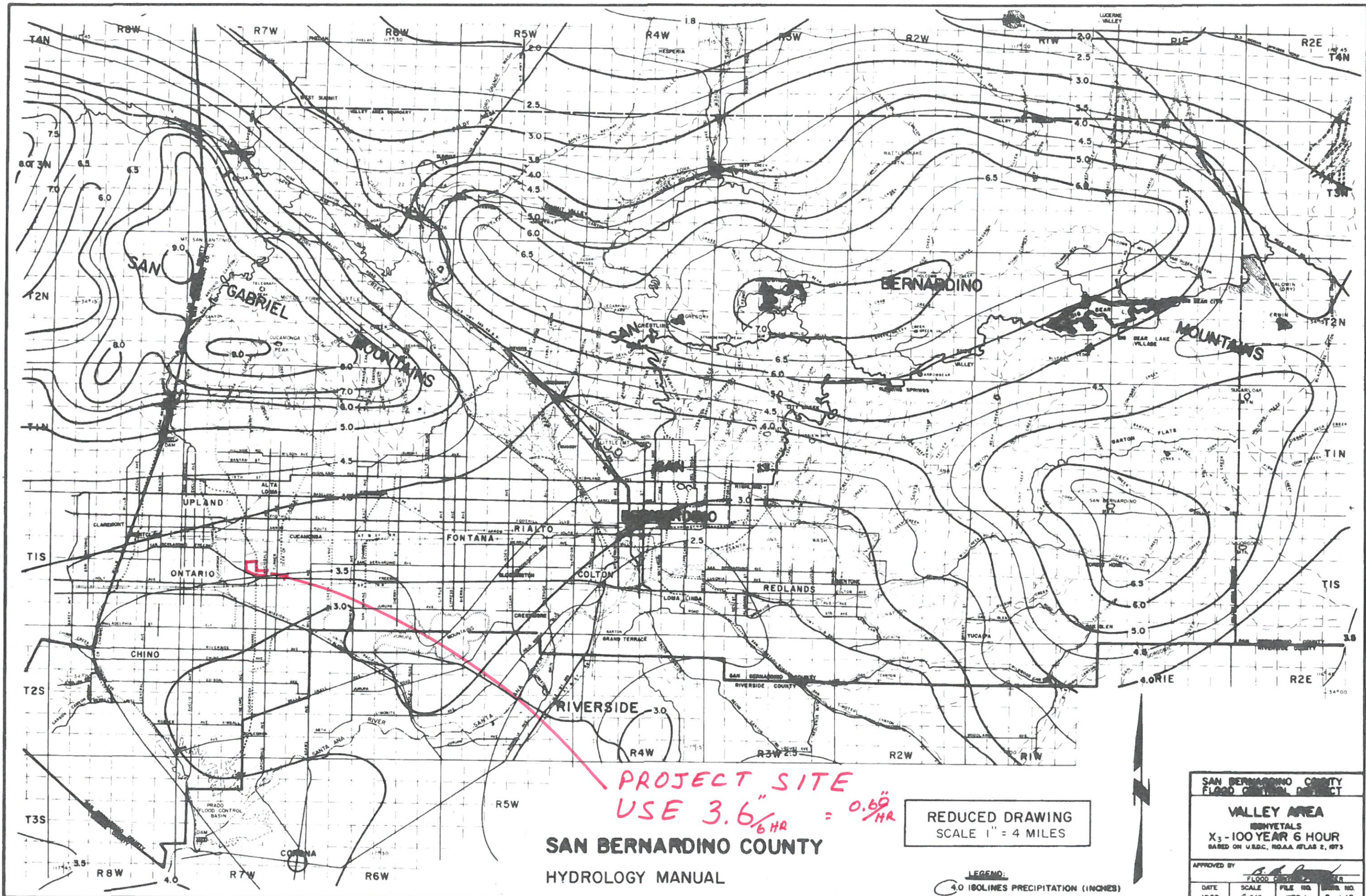
SAN BERNARDINO COUNTY
FLOOD CONTROL DISTRICT

VALLEY AREA
ISOHYETALS
Y₁₀ - 10 YEAR 1 HOUR
BASED ON U.S.D.C. NOAA ATLAS 2, 1973

APPROVED BY: *[Signature]*
FLOOD CONTROL ENGINEER

DATE	SCALE	FILE NO.	DRWG. NO.
1982	1" = 2 MI.	WRD-1	3 of 12



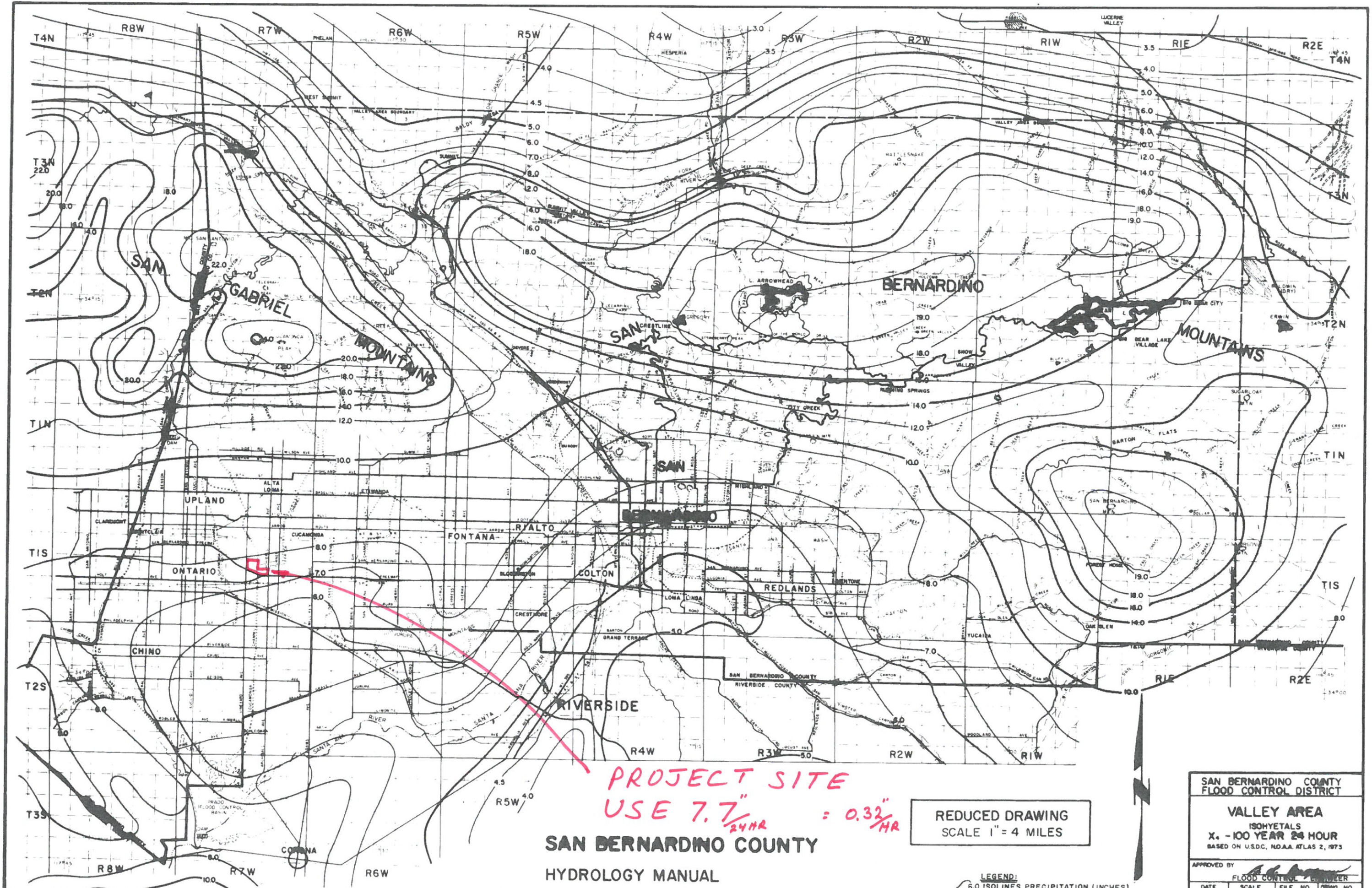


PROJECT SITE
USE 3.6" / 6 HR = 0.60" / HR
SAN BERNARDINO COUNTY
 HYDROLOGY MANUAL

REDUCED DRAWING
 SCALE 1" = 4 MILES

LEGEND:
 4.0 ISOLINES PRECIPITATION (INCHES)

SAN BERNARDINO COUNTY FLOOD CONTROL DISTRICT			
VALLEY AREA			
180VETALS			
X ₃ -100 YEAR 6 HOUR			
BASED ON U.S.D.C. NO. 44 ATLAS 2, 1973			
APPROVED BY: <i>[Signature]</i>			
DATE	SCALE	FILE NO.	DRAW. NO.
1962	1"=2 MI.	WB-1	5 of 12



*PROJECT SITE
USE 7.7" $\frac{24}{HR}$ = 0.32" \frac{HR}*

**SAN BERNARDINO COUNTY
HYDROLOGY MANUAL**

**REDUCED DRAWING
SCALE 1" = 4 MILES**

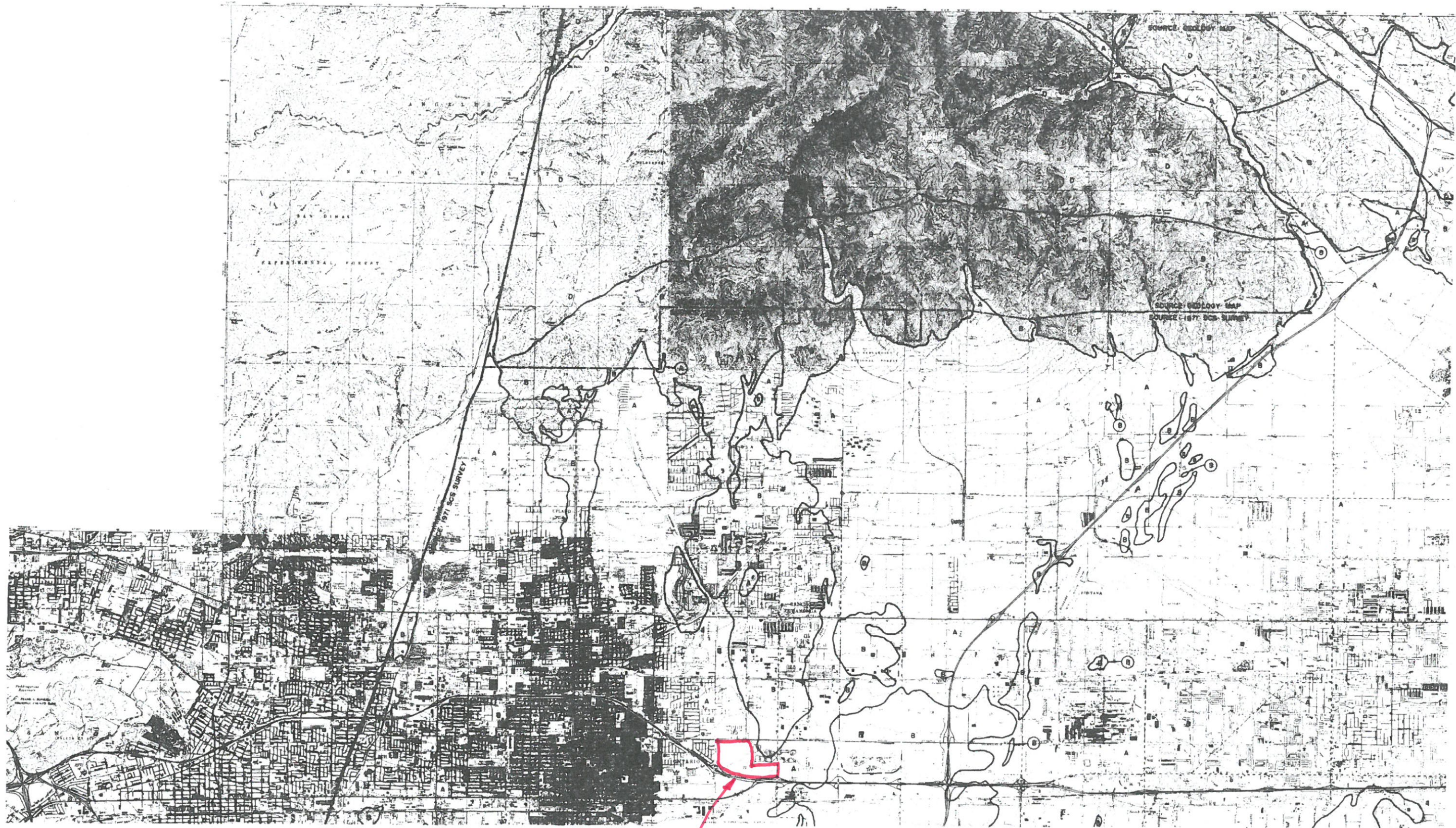
**LEGEND:
6.0 ISOLINES PRECIPITATION (INCHES)**

**SAN BERNARDINO COUNTY
FLOOD CONTROL DISTRICT**

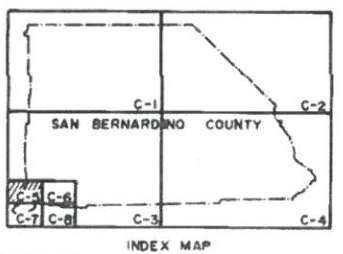
**VALLEY AREA
ISOHYETALS
X₁ - 100 YEAR 24 HOUR
BASED ON U.S.D.C. NO. AA ATLAS 2, 1973**

APPROVED BY _____
FLOOD CONTROL ENGINEER

DATE	SCALE	FILE NO.	DRWG. NO.
1982	1" = 2 MI.	WRD-1	6 of 12



SAN BERNARDINO COUNTY
 HYDROLOGY MANUAL

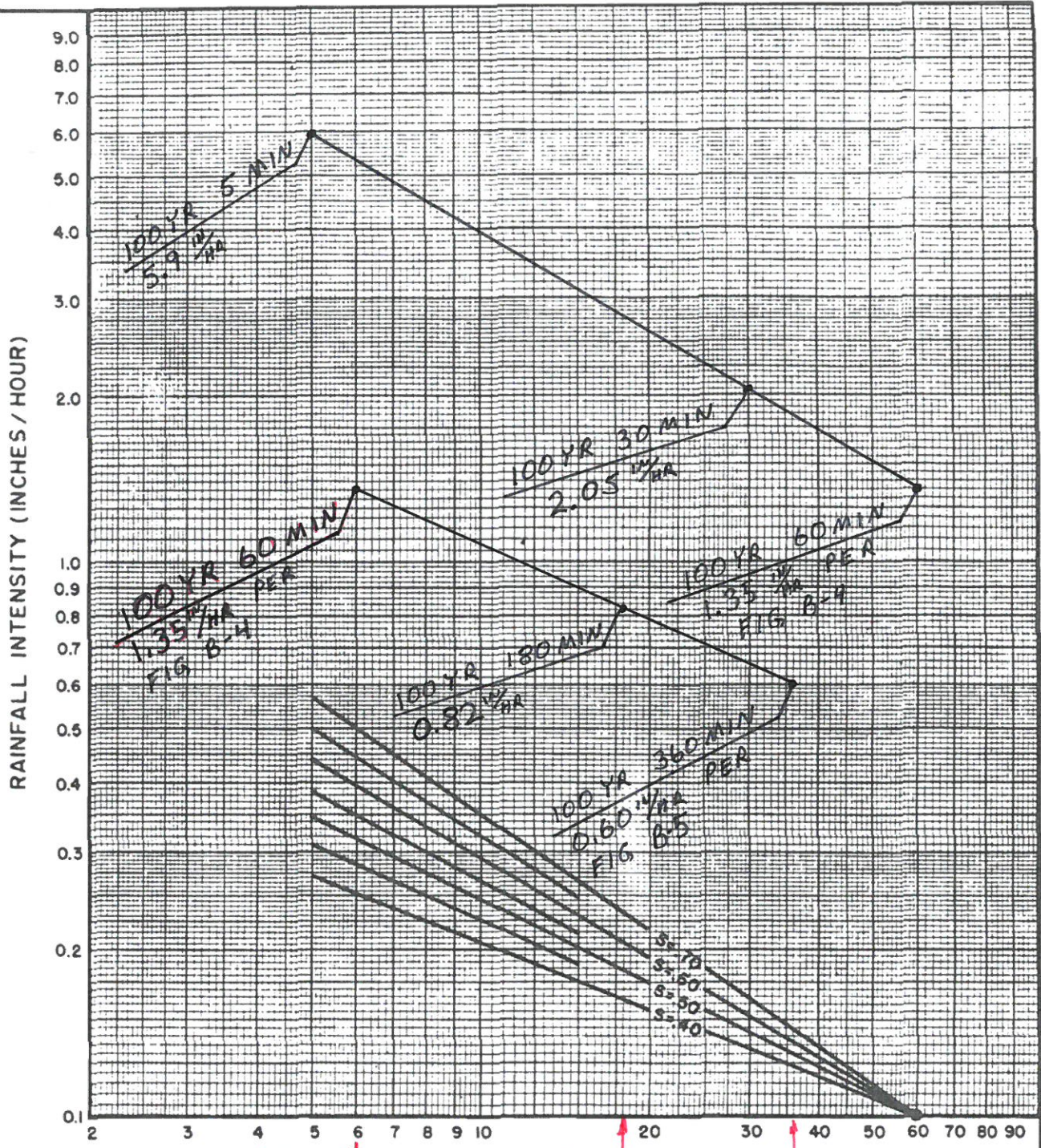


- LEGEND
- SOIL GROUP BOUNDARY
 - A SOIL GROUP DESIGNATION
 - - - BOUNDARY OF INDICATED SOURCE

SCALE REDUCED BY 1/2

*PROJECT SITE
 USE SOIL GROUP A*

**HYDROLOGIC SOILS GROUP MAP
 FOR
 SOUTHWEST-A AREA**



DESIGN STORM FREQUENCY = 100 YEARS
 ONE HOUR POINT RAINFALL = 1.35 INCHES
 LOG-LOG SLOPE = 0.60
 PROJECT LOCATION = VINEYARD & INLAND EMPIRE
CITY OF ONTARIO

SAN BERNARDINO COUNTY
 HYDROLOGY MANUAL

**INTENSITY - DURATION
 CURVES
 CALCULATION SHEET**

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION)
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Ver. 18.0 Release Date: 07/01/2011 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* MEREDITH PROPERTY *
* WATERSHED 1 *
* EXISTING CONDITION 100 YR STORM *

FILE NAME: E-W1-R.DAT
TIME/DATE OF STUDY: 13:49 04/22/2014

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/ SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- Relative Flow-Depth = 0.70 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 - (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 1000.00
ELEVATION DATA: UPSTREAM(FEET) = 1034.00 DOWNSTREAM(FEET) = 1019.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 25.917
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.234
SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
NATURAL FAIR COVER						
"GRASS"	A	16.50	0.50	1.000	70	25.92

SUBAREA AVERAGE PVIOUS LOSS RATE, F_p (INCH/HR) = 0.50
SUBAREA AVERAGE PVIOUS AREA FRACTION, A_p = 1.000
SUBAREA RUNOFF(CFS) = 25.82
TOTAL AREA(ACRES) = 16.50 PEAK FLOW RATE(CFS) = 25.82

FLOW PROCESS FROM NODE 2.00 TO NODE 3.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1019.00 DOWNSTREAM(FEET) = 1008.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1000.00 CHANNEL SLOPE = 0.0110
CHANNEL FLOW THRU SUBAREA(CFS) = 25.82
FLOW VELOCITY(FEET/SEC) = 3.37 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.95 T_c (MIN.) = 30.86
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 3.00 = 2000.00 FEET.

FLOW PROCESS FROM NODE 3.00 TO NODE 3.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<

=====

MAINLINE T_c (MIN.) = 30.86
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.012
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
NATURAL FAIR COVER					
"GRASS"	A	49.70	0.50	1.000	70

SUBAREA AVERAGE PVIOUS LOSS RATE, F_p (INCH/HR) = 0.50
SUBAREA AVERAGE PVIOUS AREA FRACTION, A_p = 1.000
SUBAREA AREA(ACRES) = 49.70 SUBAREA RUNOFF(CFS) = 67.84
EFFECTIVE AREA(ACRES) = 66.20 AREA-AVERAGED F_m (INCH/HR) = 0.50
AREA-AVERAGED F_p (INCH/HR) = 0.50 AREA-AVERAGED A_p = 1.00
TOTAL AREA(ACRES) = 66.2 PEAK FLOW RATE(CFS) = 90.36

FLOW PROCESS FROM NODE 3.00 TO NODE 4.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1008.00 DOWNSTREAM(FEET) = 997.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1000.00 CHANNEL SLOPE = 0.0110

CHANNEL FLOW THRU SUBAREA(CFS) = 90.36
FLOW VELOCITY(FEET/SEC) = 4.83 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.45 Tc(MIN.) = 34.31
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 4.00 = 3000.00 FEET.

FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 81

=====
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 34.31
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 1.888
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
NATURAL FAIR COVER
"GRASS" A 71.30 0.50 1.000 70
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.50
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA AREA(ACRES) = 71.30 SUBAREA RUNOFF(CFS) = 89.37
EFFECTIVE AREA(ACRES) = 137.50 AREA-AVERAGED Fm(INCH/HR) = 0.50
AREA-AVERAGED Fp(INCH/HR) = 0.50 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 137.5 PEAK FLOW RATE(CFS) = 172.35

FLOW PROCESS FROM NODE 4.00 TO NODE 5.00 IS CODE = 52

=====
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 997.00 DOWNSTREAM(FEET) = 984.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 900.00 CHANNEL SLOPE = 0.0144
CHANNEL FLOW THRU SUBAREA(CFS) = 172.35
FLOW VELOCITY(FEET/SEC) = 6.73 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.23 Tc(MIN.) = 36.54
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 5.00 = 3900.00 FEET.

FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 81

=====
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 36.54
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 1.818
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
NATURAL FAIR COVER
"GRASS" A 29.50 0.50 1.000 70
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.50
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA AREA(ACRES) = 29.50 SUBAREA RUNOFF(CFS) = 35.12
EFFECTIVE AREA(ACRES) = 167.00 AREA-AVERAGED Fm(INCH/HR) = 0.50
AREA-AVERAGED Fp(INCH/HR) = 0.50 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 167.0 PEAK FLOW RATE(CFS) = 198.82

=====
END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 167.0 TC(MIN.) = 36.54

EFFECTIVE AREA(ACRES) = 167.00 AREA-AVERAGED Fm(INCH/HR)= 0.50
AREA-AVERAGED Fp(INCH/HR) = 0.50 AREA-AVERAGED Ap = 1.000
PEAK FLOW RATE(CFS) = 198.82

=====
END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Ver. 18.0 Release Date: 07/01/2011 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* MEREDITH PROPERTY *
* WATERSHED 2 *
* EXISTING CONDITION 100 YR STORM *

FILE NAME: E-W2-R.DAT
TIME/DATE OF STUDY: 14:30 04/22/2014

=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

Table with 10 columns: NO., WIDTH (FT), CROSSFALL (FT), SIDE / SIDE- / WAY, HEIGHT (FT), GUTTER-GEOMETRIES: MANNING, WIDTH (FT), LIP (FT), HIKE (FT), FACTOR (n). Row 1: 1, 30.0, 20.0, 0.018/0.018/0.020, 0.67, 2.00, 0.0313, 0.167, 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- 1. Relative Flow-Depth = 0.70 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 6.00 TO NODE 7.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 850.00
ELEVATION DATA: UPSTREAM(FEET) = 1010.00 DOWNSTREAM(FEET) = 999.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 10.771
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.783
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL A 1.80 0.74 0.100 52 10.77
SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 6.01
TOTAL AREA(ACRES) = 1.80 PEAK FLOW RATE(CFS) = 6.01

FLOW PROCESS FROM NODE 7.00 TO NODE 8.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
REPRESENTATIVE SLOPE = 0.0110
STREET LENGTH(FEET) = 2300.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.76
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.42
HALFSTREET FLOOD WIDTH(FEET) = 14.65
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.79
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.18
STREET FLOW TRAVEL TIME(MIN.) = 13.75 Tc(MIN.) = 24.52
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.309

SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 5.60 0.74 0.100 52
SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 5.60 SUBAREA RUNOFF(CFS) = 11.27
EFFECTIVE AREA(ACRES) = 7.40 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 7.4 PEAK FLOW RATE(CFS) = 14.89

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.45 HALFSTREET FLOOD WIDTH(FEET) = 16.13
FLOW VELOCITY(FEET/SEC.) = 2.96 DEPTH*VELOCITY(FT*FT/SEC.) = 1.33

LONGEST FLOWPATH FROM NODE 6.00 TO NODE 8.00 = 3150.00 FEET.

=====
END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 7.4 TC (MIN.) = 24.52
EFFECTIVE AREA (ACRES) = 7.40 AREA-AVERAGED F_m (INCH/HR) = 0.07
AREA-AVERAGED F_p (INCH/HR) = 0.74 AREA-AVERAGED A_p = 0.100
PEAK FLOW RATE (CFS) = 14.89
=====

=====
END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Ver. 18.0 Release Date: 07/01/2011 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****

- * MEREDITH PROPERTY
* WATERSHED 3
* EXISTING CONDITION 100 YR STORM

FILE NAME: E-W3-R.DAT
TIME/DATE OF STUDY: 14:18 04/22/2014

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

Table with columns: NO., WIDTH (FT), CROSSFALL (FT), SIDE / SIDE/ WAY, HEIGHT (FT), WIDTH (FT), LIP (FT), HIKE (FT), MANNING FACTOR (n). Row 1: 1, 30.0, 20.0, 0.018/0.018/0.020, 0.67, 2.00, 0.0313, 0.167, 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- 1. Relative Flow-Depth = 0.70 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 9.00 TO NODE 10.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 1000.00
ELEVATION DATA: UPSTREAM(FEET) = 1010.00 DOWNSTREAM(FEET) = 995.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 25.917
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.234
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
NATURAL FAIR COVER
"GRASS" A 3.40 0.50 1.000 70 25.92
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.50
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA RUNOFF(CFS) = 5.32
TOTAL AREA(ACRES) = 3.40 PEAK FLOW RATE(CFS) = 5.32

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<

ELEVATION DATA: UPSTREAM(FEET) = 995.00 DOWNSTREAM(FEET) = 973.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 2280.00 CHANNEL SLOPE = 0.0096
CHANNEL FLOW THRU SUBAREA(CFS) = 5.32
FLOW VELOCITY(FEET/SEC) = 2.10 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 18.07 Tc(MIN.) = 43.99
LONGEST FLOWPATH FROM NODE 9.00 TO NODE 11.00 = 3280.00 FEET.

FLOW PROCESS FROM NODE 11.00 TO NODE 11.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 43.99
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 1.626
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
NATURAL FAIR COVER
"GRASS" A 25.00 0.50 1.000 70
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.50
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA AREA(ACRES) = 25.00 SUBAREA RUNOFF(CFS) = 25.46
EFFECTIVE AREA(ACRES) = 28.40 AREA-AVERAGED Fm(INCH/HR) = 0.50
AREA-AVERAGED Fp(INCH/HR) = 0.50 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 28.4 PEAK FLOW RATE(CFS) = 28.92

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 28.4 TC(MIN.) = 43.99
EFFECTIVE AREA(ACRES) = 28.40 AREA-AVERAGED Fm(INCH/HR) = 0.50
AREA-AVERAGED Fp(INCH/HR) = 0.50 AREA-AVERAGED Ap = 1.000
PEAK FLOW RATE(CFS) = 28.92

END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Analysis prepared by:

***** DESCRIPTION OF STUDY *****

* MEREDITH PROPERTY *
* WATERSHED 4 *
* EXISTING CONDITION 100 YR STORM *

FILE NAME: E-W4-R.DAT
TIME/DATE OF STUDY: 14:40 04/22/2014

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL IN- / OUT- / SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES LIP (FT)	MANNING HIKE (FT)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.70 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 12.00 TO NODE 13.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 750.00
ELEVATION DATA: UPSTREAM(FEET) = 985.00 DOWNSTREAM(FEET) = 974.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 23.204
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.387
SUBAREA T_c AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ LAND USE SCS SOIL GROUP AREA (ACRES) F_p (INCH/HR) A_p (DECIMAL) SCS CN T_c (MIN.)
NATURAL FAIR COVER
"GRASS" A 3.70 0.50 1.000 70 23.20
SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.50
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000
SUBAREA RUNOFF(CFS) = 6.30
TOTAL AREA(ACRES) = 3.70 PEAK FLOW RATE(CFS) = 6.30

=====

END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 3.7 T_c (MIN.) = 23.20
EFFECTIVE AREA(ACRES) = 3.70 AREA-AVERAGED F_m (INCH/HR) = 0.50
AREA-AVERAGED F_p (INCH/HR) = 0.50 AREA-AVERAGED A_p = 1.000
PEAK FLOW RATE(CFS) = 6.30

=====

END OF RATIONAL METHOD ANALYSIS

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Analysis prepared by:

***** DESCRIPTION OF STUDY *****

* MEREDITH PROPERTY *
* WATERSHED 5 *
* EXISTING CONDITION 100 YR STORM *

FILE NAME: E-W5-R.DAT
TIME/DATE OF STUDY: 14:29 04/28/2014

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

Table with columns: NO., WIDTH (FT), CROSSFALL (FT), SIDE / SIDE- / WAY, HEIGHT (FT), WIDTH (FT), LIP (FT), HIKE (FT), MANNING FACTOR (n). Row 1: 1, 30.0, 20.0, 0.018/0.018/0.020, 0.67, 2.00, 0.0313, 0.167, 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- 1. Relative Flow-Depth = 0.70 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)

SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 14.00 TO NODE 15.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 730.00
ELEVATION DATA: UPSTREAM(FEET) = 991.00 DOWNSTREAM(FEET) = 985.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 25.773
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.241
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
NATURAL FAIR COVER
"GRASS" A 7.00 0.50 1.000 70 25.77
SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.50
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 1.000
SUBAREA RUNOFF(CFS) = 11.00
TOTAL AREA(ACRES) = 7.00 PEAK FLOW RATE(CFS) = 11.00

FLOW PROCESS FROM NODE 15.00 TO NODE 16.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<

ELEVATION DATA: UPSTREAM(FEET) = 985.00 DOWNSTREAM(FEET) = 980.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 950.00 CHANNEL SLOPE = 0.0053
CHANNEL FLOW THRU SUBAREA(CFS) = 11.00
FLOW VELOCITY(FEET/SEC) = 1.86 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 8.52 Tc(MIN.) = 34.30
LONGEST FLOWPATH FROM NODE 14.00 TO NODE 16.00 = 1680.00 FEET.

FLOW PROCESS FROM NODE 16.00 TO NODE 16.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 34.30
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 1.888
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
NATURAL FAIR COVER
"GRASS" A 14.90 0.50 1.000 70
SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.50
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 1.000
SUBAREA AREA(ACRES) = 14.90 SUBAREA RUNOFF(CFS) = 18.68
EFFECTIVE AREA(ACRES) = 21.90 AREA-AVERAGED Fm(INCH/HR) = 0.50
AREA-AVERAGED Fp(INCH/HR) = 0.50 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 21.9 PEAK FLOW RATE(CFS) = 27.46

FLOW PROCESS FROM NODE 16.00 TO NODE 16.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 34.30

RAINFALL INTENSITY (INCH/HR) = 1.89
 AREA-AVERAGED Fm (INCH/HR) = 0.50
 AREA-AVERAGED Fp (INCH/HR) = 0.50
 AREA-AVERAGED Ap = 1.00
 EFFECTIVE STREAM AREA (ACRES) = 21.90
 TOTAL STREAM AREA (ACRES) = 21.90
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 27.46

 FLOW PROCESS FROM NODE 17.00 TO NODE 16.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 1000.00
 ELEVATION DATA: UPSTREAM (FEET) = 988.00 DOWNSTREAM (FEET) = 980.00

Tc = K * [(LENGTH** 3.00) / (ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 12.655
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.435
 SUBAREA Tc AND LOSS RATE DATA (AMC III):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
 COMMERCIAL A 2.70 0.74 0.100 52 12.65
 SUBAREA AVERAGE PVIOUS LOSS RATE, Fp (INCH/HR) = 0.74
 SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA RUNOFF (CFS) = 8.17
 TOTAL AREA (ACRES) = 2.70 PEAK FLOW RATE (CFS) = 8.17

 FLOW PROCESS FROM NODE 16.00 TO NODE 16.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION (MIN.) = 12.65
 RAINFALL INTENSITY (INCH/HR) = 3.43
 AREA-AVERAGED Fm (INCH/HR) = 0.07
 AREA-AVERAGED Fp (INCH/HR) = 0.74
 AREA-AVERAGED Ap = 0.10
 EFFECTIVE STREAM AREA (ACRES) = 2.70
 TOTAL STREAM AREA (ACRES) = 2.70
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 8.17

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	27.46	34.30	1.888	0.50 (0.50)	1.00	21.9	14.00
2	8.17	12.65	3.435	0.74 (0.07)	0.10	2.7	17.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	27.46	34.30	1.888	0.50 (0.50)	1.00	21.9	14.00
2	8.17	12.65	3.435	0.74 (0.07)	0.10	2.7	17.00

1	29.54	12.65	3.435	0.50 (0.39)	0.77	10.8	17.00
2	31.87	34.30	1.888	0.50 (0.45)	0.90	24.6	14.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE (CFS) = 31.87 Tc (MIN.) = 34.30
 EFFECTIVE AREA (ACRES) = 24.60 AREA-AVERAGED Fm (INCH/HR) = 0.45
 AREA-AVERAGED Fp (INCH/HR) = 0.50 AREA-AVERAGED Ap = 0.90
 TOTAL AREA (ACRES) = 24.6
 LONGEST FLOWPATH FROM NODE 14.00 TO NODE 16.00 = 1680.00 FEET.

 FLOW PROCESS FROM NODE 16.00 TO NODE 18.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

REPRESENTATIVE SLOPE = 0.0100
 FLOW LENGTH (FEET) = 100.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 20.7 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 8.84
 ESTIMATED PIPE DIAMETER (INCH) = 30.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 31.87
 PIPE TRAVEL TIME (MIN.) = 0.19 Tc (MIN.) = 34.48
 LONGEST FLOWPATH FROM NODE 14.00 TO NODE 18.00 = 1780.00 FEET.

 FLOW PROCESS FROM NODE 18.00 TO NODE 18.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 34.48
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 1.882
 SUBAREA LOSS RATE DATA (AMC III):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 COMMERCIAL A 3.40 0.74 0.100 52
 SUBAREA AVERAGE PVIOUS LOSS RATE, Fp (INCH/HR) = 0.74
 SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA (ACRES) = 3.40 SUBAREA RUNOFF (CFS) = 5.53
 EFFECTIVE AREA (ACRES) = 28.00 AREA-AVERAGED Fm (INCH/HR) = 0.40
 AREA-AVERAGED Fp (INCH/HR) = 0.50 AREA-AVERAGED Ap = 0.80
 TOTAL AREA (ACRES) = 28.0 PEAK FLOW RATE (CFS) = 37.27

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	39.43	12.85	3.404	0.51 (0.31)	0.61	14.2	17.00
2	37.27	34.48	1.882	0.50 (0.40)	0.80	28.0	14.00

NEW PEAK FLOW DATA ARE:
 PEAK FLOW RATE (CFS) = 39.43 Tc (MIN.) = 12.85
 AREA-AVERAGED Fm (INCH/HR) = 0.31 AREA-AVERAGED Fp (INCH/HR) = 0.51
 AREA-AVERAGED Ap = 0.61 EFFECTIVE AREA (ACRES) = 14.18

 FLOW PROCESS FROM NODE 18.00 TO NODE 19.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
 >>>>TRAVELTIME THRU SUBAREA<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 979.00 DOWNSTREAM(FEET) = 975.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.0067
CHANNEL FLOW THRU SUBAREA(CFS) = 39.43
FLOW VELOCITY(FEET/SEC) = 2.95 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.39 Tc(MIN.) = 16.23
LONGEST FLOWPATH FROM NODE 14.00 TO NODE 19.00 = 2380.00 FEET.

```

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*****
FLOW PROCESS FROM NODE 19.00 TO NODE 19.00 IS CODE = 81

```

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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

```

```

=====
MAINLINE Tc(MIN.) = 16.23
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.958
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap      SCS
LAND USE              GROUP  (ACRES)  (INCH/HR) (DECIMAL) CN
NATURAL FAIR COVER
"GRASS"                A      22.40    0.50     1.000   70
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.50
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA AREA(ACRES) = 22.40 SUBAREA RUNOFF(CFS) = 49.65
EFFECTIVE AREA(ACRES) = 36.58 AREA-AVERAGED Fm(INCH/HR) = 0.42
AREA-AVERAGED Fp(INCH/HR) = 0.50 AREA-AVERAGED Ap = 0.85
TOTAL AREA(ACRES) = 50.4 PEAK FLOW RATE(CFS) = 83.40
=====

```

```

END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 50.4 TC(MIN.) = 16.23
EFFECTIVE AREA(ACRES) = 36.58 AREA-AVERAGED Fm(INCH/HR)= 0.42
AREA-AVERAGED Fp(INCH/HR) = 0.50 AREA-AVERAGED Ap = 0.850
PEAK FLOW RATE(CFS) = 83.40

```

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	83.40	16.23	2.958	0.50 (0.42)	0.85	36.6	17.00
2	60.49	37.93	1.778	0.50 (0.44)	0.89	50.4	14.00

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END OF RATIONAL METHOD ANALYSIS

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Ver. 18.0 Release Date: 07/01/2011 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* MEREDITH PROPERTY *
* WATERSHED 1 *
* PROPOSED CONDITION 100 YR STORM *

FILE NAME: P-W1-R.DAT
TIME/DATE OF STUDY: 07:57 04/23/2014

=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

Table with 10 columns: NO., WIDTH (FT), CROSSFALL (FT), SIDE / SIDE- / WAY, HEIGHT (FT), WIDTH (FT), LIP (FT), HIKE (FT), FACTOR (n). Row 1: 1, 30.0, 20.0, 0.018/0.018/0.020, 0.67, 2.00, 0.0313, 0.167, 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- 1. Relative Flow-Depth = 0.70 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 1000.00
ELEVATION DATA: UPSTREAM(FEET) = 1034.00 DOWNSTREAM(FEET) = 1023.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.874
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.568
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL A 7.00 0.74 0.100 52 11.87
SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 22.01
TOTAL AREA(ACRES) = 7.00 PEAK FLOW RATE(CFS) = 22.01

FLOW PROCESS FROM NODE 2.00 TO NODE 3.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
REPRESENTATIVE SLOPE = 0.0140
STREET LENGTH(FEET) = 1080.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 39.44
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.57
HALFSTREET FLOOD WIDTH(FEET) = 22.77
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.09
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.33
STREET FLOW TRAVEL TIME(MIN.) = 4.40 Tc(MIN.) = 16.28
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.953

SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 13.40 0.74 0.100 52
SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 13.40 SUBAREA RUNOFF(CFS) = 34.72
EFFECTIVE AREA(ACRES) = 20.40 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 20.4 PEAK FLOW RATE(CFS) = 52.85

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.62 HALFSTREET FLOOD WIDTH(FEET) = 25.51
FLOW VELOCITY(FEET/SEC.) = 4.40 DEPTH*VELOCITY(FT*FT/SEC.) = 2.72

LONGEST FLOWPATH FROM NODE 1.00 TO NODE 3.00 = 2080.00 FEET.

FLOW PROCESS FROM NODE 3.00 TO NODE 4.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

REPRESENTATIVE SLOPE = 0.0130
STREET LENGTH(FEET) = 400.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 88.26

STREET FLOWING FULL

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.72

HALFSTREET FLOOD WIDTH(FEET) = 32.71

AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.91

PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.54

STREET FLOW TRAVEL TIME(MIN.) = 1.36 Tc(MIN.) = 17.64

* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.814

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	28.70	0.74	0.100	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 28.70 SUBAREA RUNOFF(CFS) = 70.78

EFFECTIVE AREA(ACRES) = 49.10 AREA-AVERAGED Fm(INCH/HR) = 0.07

AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10

TOTAL AREA(ACRES) = 49.1 PEAK FLOW RATE(CFS) = 121.09

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.78 HALFSTREET FLOOD WIDTH(FEET) = 35.76

FLOW VELOCITY(FEET/SEC.) = 5.47 DEPTH*VELOCITY(FT*FT/SEC.) = 4.28

*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,

AND L = 400.0 FT WITH ELEVATION-DROP = 5.2 FT, IS 115.2 CFS,

WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 4.00

LONGEST FLOWPATH FROM NODE 1.00 TO NODE 4.00 = 2480.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 49.1 TC(MIN.) = 17.64

EFFECTIVE AREA(ACRES) = 49.10 AREA-AVERAGED Fm(INCH/HR) = 0.07

AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.100

PEAK FLOW RATE(CFS) = 121.09

END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* MEREDITH PROPERTY *
* WATERSHED 2 *
* PROPOSED CONDITION 100 YR STORM *

FILE NAME: P-W2-R.DAT
TIME/DATE OF STUDY: 08:12 04/23/2014

=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

Table with 10 columns: NO., WIDTH (FT), CROSSFALL (FT), SIDE / SIDE- / WAY, HEIGHT (FT), WIDTH (FT), LIP (FT), HIKE (FT), FACTOR (n). Row 1: 1, 30.0, 20.0, 0.018/0.018/0.020, 0.67, 2.00, 0.0313, 0.167, 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- 1. Relative Flow-Depth = 0.70 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 5.00 TO NODE 6.00 IS CODE = 21
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 1000.00
ELEVATION DATA: UPSTREAM(FEET) = 1028.00 DOWNSTREAM(FEET) = 1022.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 13.404
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.318
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL A 8.30 0.74 0.100 52 13.40
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 24.23
TOTAL AREA(ACRES) = 8.30 PEAK FLOW RATE(CFS) = 24.23

FLOW PROCESS FROM NODE 6.00 TO NODE 7.00 IS CODE = 62
=====

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
REPRESENTATIVE SLOPE = 0.0100
STREET LENGTH(FEET) = 1430.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 56.10

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.66
HALFSTREET FLOOD WIDTH(FEET) = 27.93
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.92
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.59
STREET FLOW TRAVEL TIME(MIN.) = 6.08 Tc(MIN.) = 19.49
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.651

SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 27.30 0.74 0.100 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 27.30 SUBAREA RUNOFF(CFS) = 63.31
EFFECTIVE AREA(ACRES) = 35.60 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 35.6 PEAK FLOW RATE(CFS) = 82.55

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.73 HALFSTREET FLOOD WIDTH(FEET) = 33.26
FLOW VELOCITY(FEET/SEC.) = 4.42 DEPTH*VELOCITY(FT*FT/SEC.) = 3.23

*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,
AND L = 1430.0 FT WITH ELEVATION-DROP = 14.3 FT, IS 77.7 CFS,
WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 7.00
LONGEST FLOWPATH FROM NODE 5.00 TO NODE 7.00 = 2430.00 FEET.

FLOW PROCESS FROM NODE 7.00 TO NODE 8.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

REPRESENTATIVE SLOPE = 0.0080
STREET LENGTH(FEET) = 1830.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 103.55
STREET FLOWING FULL

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.80
HALFSTREET FLOOD WIDTH(FEET) = 36.68
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.41
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.53
STREET FLOW TRAVEL TIME(MIN.) = 6.91 Tc(MIN.) = 26.40
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.209

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	21.80	0.74	0.100	52

SUBAREA AVERAGE PVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 21.80 SUBAREA RUNOFF(CFS) = 41.89
EFFECTIVE AREA(ACRES) = 57.40 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 57.4 PEAK FLOW RATE(CFS) = 110.30

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.81 HALFSTREET FLOOD WIDTH(FEET) = 37.35
FLOW VELOCITY(FEET/SEC.) = 4.51 DEPTH*VELOCITY(FT*FT/SEC.) = 3.67

*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,
AND L = 1830.0 FT WITH ELEVATION-DROP = 14.6 FT, IS 56.8 CFS,
WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 8.00
LONGEST FLOWPATH FROM NODE 5.00 TO NODE 8.00 = 4260.00 FEET.

=====

END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 57.4 TC(MIN.) = 26.40
EFFECTIVE AREA(ACRES) = 57.40 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.100
PEAK FLOW RATE(CFS) = 110.30
=====

=====

END OF RATIONAL METHOD ANALYSIS

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Ver. 18.0 Release Date: 07/01/2011 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* MEREDITH PROPERTY *
* WATERSHED 3 *
* PROPOSED CONDITION 100 YR STORM *

FILE NAME: P-W3-R.DAT
TIME/DATE OF STUDY: 08:21 04/23/2014

=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL
HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- 1. Relative Flow-Depth = 0.70 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 9.00 TO NODE 10.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 830.00
ELEVATION DATA: UPSTREAM(FEET) = 1020.00 DOWNSTREAM(FEET) = 1004.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.851
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.991
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL A 10.70 0.74 0.100 52 9.85
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 37.72
TOTAL AREA(ACRES) = 10.70 PEAK FLOW RATE(CFS) = 37.72

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
REPRESENTATIVE SLOPE = 0.0060
STREET LENGTH(FEET) = 1720.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 77.23
STREET FLOWING FULL

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.77
HALFSTREET FLOOD WIDTH(FEET) = 35.09
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.64
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.80
STREET FLOW TRAVEL TIME(MIN.) = 7.87 Tc(MIN.) = 17.72
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.807

SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 31.60 0.74 0.100 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 31.60 SUBAREA RUNOFF(CFS) = 77.71
EFFECTIVE AREA(ACRES) = 42.30 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 42.3 PEAK FLOW RATE(CFS) = 104.02

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.83 HALFSTREET FLOOD WIDTH(FEET) = 38.33

FLOW VELOCITY (FEET/SEC.) = 4.01 DEPTH*VELOCITY (FT*FT/SEC.) = 3.34
*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,
AND L = 1720.0 FT WITH ELEVATION-DROP = 10.3 FT, IS 80.7 CFS,
WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 11.00
LONGEST FLOWPATH FROM NODE 9.00 TO NODE 11.00 = 2550.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 42.3 TC (MIN.) = 17.72
EFFECTIVE AREA (ACRES) = 42.30 AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.100
PEAK FLOW RATE (CFS) = 104.02

=====

END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Ver. 18.0 Release Date: 07/01/2011 License ID 1264

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* MEREDITH PROPERTY *
* WATERSHED 4 *
* PROPOSED CONDITION 100 YR STORM *

FILE NAME: P-W4-R.DAT
TIME/DATE OF STUDY: 08:27 04/23/2014

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL IN- / OUT- / SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES LIP (FT)	MANNING HIKE (FT)	STREETS FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.70 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 12.00 TO NODE 13.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 1000.00
ELEVATION DATA: UPSTREAM(FEET) = 1015.00 DOWNSTREAM(FEET) = 1004.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 11.874
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.568
SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	2.90	0.74	0.100	52	11.87

SUBAREA AVERAGE PVIOUS LOSS RATE, F_p (INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, A_p = 0.100
SUBAREA RUNOFF(CFS) = 9.12
TOTAL AREA(ACRES) = 2.90 PEAK FLOW RATE(CFS) = 9.12

FLOW PROCESS FROM NODE 13.00 TO NODE 14.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

REPRESENTATIVE SLOPE = 0.0090
STREET LENGTH(FEET) = 2300.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.14
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.48
HALFSTREET FLOOD WIDTH(FEET) = 17.85
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.82
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.36
STREET FLOW TRAVEL TIME(MIN.) = 13.59 T_c (MIN.) = 25.47
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.257

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
COMMERCIAL	A	8.00	0.74	0.100	52

SUBAREA AVERAGE PVIOUS LOSS RATE, F_p (INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, A_p = 0.100
SUBAREA AREA(ACRES) = 8.00 SUBAREA RUNOFF(CFS) = 15.72
EFFECTIVE AREA(ACRES) = 10.90 AREA-AVERAGED F_m (INCH/HR) = 0.07
AREA-AVERAGED F_p (INCH/HR) = 0.74 AREA-AVERAGED A_p = 0.10
TOTAL AREA(ACRES) = 10.9 PEAK FLOW RATE(CFS) = 21.42

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.51 HALFSTREET FLOOD WIDTH(FEET) = 19.49
FLOW VELOCITY(FEET/SEC.) = 2.99 DEPTH*VELOCITY(FT*FT/SEC.) = 1.52

LONGEST FLOWPATH FROM NODE 12.00 TO NODE 14.00 = 3300.00 FEET.

=====
END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 10.9 TC (MIN.) = 25.47
EFFECTIVE AREA (ACRES) = 10.90 AREA-AVERAGED F_m (INCH/HR) = 0.07
AREA-AVERAGED F_p (INCH/HR) = 0.74 AREA-AVERAGED A_p = 0.100
PEAK FLOW RATE (CFS) = 21.42
=====

=====
END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* MEREDITH PROPERTY *
* WATERSHED 5 *
* PROPOSED CONDITION 100 YR STORM *

FILE NAME: P-W5-R.DAT
TIME/DATE OF STUDY: 08:33 04/23/2014

=====
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL
HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)
=== =====
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.70 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 15.00 TO NODE 16.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 1000.00
ELEVATION DATA: UPSTREAM(FEET) = 1014.00 DOWNSTREAM(FEET) = 1000.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.315
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.673
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL A 12.60 0.74 0.100 52 11.31
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 40.81
TOTAL AREA(ACRES) = 12.60 PEAK FLOW RATE(CFS) = 40.81

FLOW PROCESS FROM NODE 16.00 TO NODE 17.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
REPRESENTATIVE SLOPE = 0.0110
STREET LENGTH(FEET) = 2400.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 76.52
STREET FLOWING FULL

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.71
HALFSTREET FLOOD WIDTH(FEET) = 32.22
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.42
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.14
STREET FLOW TRAVEL TIME(MIN.) = 9.06 Tc(MIN.) = 20.37
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.581

SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 31.10 0.74 0.100 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 31.10 SUBAREA RUNOFF(CFS) = 70.16
EFFECTIVE AREA(ACRES) = 43.70 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 43.7 PEAK FLOW RATE(CFS) = 98.59

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.76 HALFSTREET FLOOD WIDTH(FEET) = 34.54

FLOW VELOCITY (FEET/SEC.) = 4.83 DEPTH*VELOCITY (FT*FT/SEC.) = 3.66
*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,
AND L = 2400.0 FT WITH ELEVATION-DROP = 26.4 FT, IS 78.9 CFS,
WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 17.00
LONGEST FLOWPATH FROM NODE 15.00 TO NODE 17.00 = 3400.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 43.7 TC (MIN.) = 20.37
EFFECTIVE AREA (ACRES) = 43.70 AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.100
PEAK FLOW RATE (CFS) = 98.59

=====

END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* MEREDITH PROPERTY *
* WATERSHED 6 *
* PROPOSED CONDITION 100 YR STORM *

FILE NAME: P-W6-R.DAT
TIME/DATE OF STUDY: 14:42 04/28/2014

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.930
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.350
COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.3500
SLOPE OF INTENSITY DURATION CURVE = 0.6000

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL IN- / OUT- / SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES LIP (FT)	MANNING HIKE (FT)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.70 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 18.00 TO NODE 19.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 700.00
ELEVATION DATA: UPSTREAM(FEET) = 991.00 DOWNSTREAM(FEET) = 985.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 10.822
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.773
SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	A	6.80	0.74	0.100	52	10.82

SUBAREA AVERAGE PVIOUS LOSS RATE, F_p (INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, A_p = 0.100
SUBAREA RUNOFF(CFS) = 22.63
TOTAL AREA(ACRES) = 6.80 PEAK FLOW RATE(CFS) = 22.63

FLOW PROCESS FROM NODE 19.00 TO NODE 20.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

REPRESENTATIVE SLOPE = 0.0060
STREET LENGTH(FEET) = 950.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 41.90
STREET FLOW SPLITS OVER STREET-CROWN
FULL DEPTH(FEET) = 0.70 FLOOD WIDTH(FEET) = 31.58
FULL HALF-STREET VELOCITY(FEET/SEC.) = 3.18
SPLIT DEPTH(FEET) = 0.60 SPLIT FLOOD WIDTH(FEET) = 24.57
SPLIT FLOW(CFS) = 15.64 SPLIT VELOCITY(FEET/SEC.) = 2.80
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.70
HALFSTREET FLOOD WIDTH(FEET) = 31.58
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.18
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.22
STREET FLOW TRAVEL TIME(MIN.) = 4.98 T_c (MIN.) = 15.80
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.006

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
COMMERCIAL	A	14.60	0.74	0.100	52

SUBAREA AVERAGE PVIOUS LOSS RATE, F_p (INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, A_p = 0.100
SUBAREA AREA(ACRES) = 14.60 SUBAREA RUNOFF(CFS) = 38.53
EFFECTIVE AREA(ACRES) = 21.40 AREA-AVERAGED F_m (INCH/HR) = 0.07
AREA-AVERAGED F_p (INCH/HR) = 0.74 AREA-AVERAGED A_p = 0.10

TOTAL AREA (ACRES) = 21.4 PEAK FLOW RATE (CFS) = 56.47

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.71 HALFSTREET FLOOD WIDTH (FEET) = 32.16
FLOW VELOCITY (FEET/SEC.) = 3.27 DEPTH*VELOCITY (FT*FT/SEC.) = 2.32

*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,
AND L = 950.0 FT WITH ELEVATION-DROP = 5.7 FT, IS 43.2 CFS,
WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 20.00
LONGEST FLOWPATH FROM NODE 18.00 TO NODE 20.00 = 1650.00 FEET.

FLOW PROCESS FROM NODE 20.00 TO NODE 20.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION (MIN.) = 15.80
RAINFALL INTENSITY (INCH/HR) = 3.01
AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.74
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA (ACRES) = 21.40
TOTAL STREAM AREA (ACRES) = 21.40
PEAK FLOW RATE (CFS) AT CONFLUENCE = 56.47

FLOW PROCESS FROM NODE 21.00 TO NODE 20.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 1000.00
ELEVATION DATA: UPSTREAM (FEET) = 988.00 DOWNSTREAM (FEET) = 980.00

Tc = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 12.655
* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.435
SUBAREA Tc AND LOSS RATE DATA (AMC III):
DEVELOPMENT TYPE/ SCSSOIL AREA Fp Ap SCSS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL A 2.70 0.74 0.100 52 12.65
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF (CFS) = 8.17
TOTAL AREA (ACRES) = 2.70 PEAK FLOW RATE (CFS) = 8.17

FLOW PROCESS FROM NODE 20.00 TO NODE 20.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION (MIN.) = 12.65
RAINFALL INTENSITY (INCH/HR) = 3.43
AREA-AVERAGED Fm (INCH/HR) = 0.07

AREA-AVERAGED Fp (INCH/HR) = 0.74
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA (ACRES) = 2.70
TOTAL STREAM AREA (ACRES) = 2.70
PEAK FLOW RATE (CFS) AT CONFLUENCE = 8.17

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	56.47	15.80	3.006	0.74 (0.07)	0.10	21.4	18.00
2	8.17	12.65	3.435	0.74 (0.07)	0.10	2.7	21.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	60.01	12.65	3.435	0.74 (0.07)	0.10	19.8	21.00
2	63.60	15.80	3.006	0.74 (0.07)	0.10	24.1	18.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE (CFS) = 63.60 Tc (MIN.) = 15.80
EFFECTIVE AREA (ACRES) = 24.10 AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA (ACRES) = 24.1
LONGEST FLOWPATH FROM NODE 18.00 TO NODE 20.00 = 1650.00 FEET.

FLOW PROCESS FROM NODE 20.00 TO NODE 22.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

REPRESENTATIVE SLOPE = 0.0100
FLOW LENGTH (FEET) = 100.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 26.7 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 10.52
ESTIMATED PIPE DIAMETER (INCH) = 39.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 63.60
PIPE TRAVEL TIME (MIN.) = 0.16 Tc (MIN.) = 15.96
LONGEST FLOWPATH FROM NODE 18.00 TO NODE 22.00 = 1750.00 FEET.

FLOW PROCESS FROM NODE 22.00 TO NODE 22.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 15.96
* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 2.988
SUBAREA LOSS RATE DATA (AMC III):
DEVELOPMENT TYPE/ SCSSOIL AREA Fp Ap SCSS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 4.60 0.74 0.100 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA (ACRES) = 4.60 SUBAREA RUNOFF (CFS) = 12.07
EFFECTIVE AREA (ACRES) = 28.70 AREA-AVERAGED Fm (INCH/HR) = 0.07

AREA-AVERAGED Fp (INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA (ACRES) = 28.7 PEAK FLOW RATE (CFS) = 75.28

FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

REPRESENTATIVE SLOPE = 0.0070
FLOW LENGTH (FEET) = 600.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 42.0 INCH PIPE IS 32.4 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 9.44
ESTIMATED PIPE DIAMETER (INCH) = 42.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 75.28
PIPE TRAVEL TIME (MIN.) = 1.06 Tc (MIN.) = 17.02
LONGEST FLOWPATH FROM NODE 18.00 TO NODE 23.00 = 2350.00 FEET.

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 17.02
* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 2.875
SUBAREA LOSS RATE DATA (AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 25.40 0.74 0.100 52
SUBAREA AVERAGE PVIOUS LOSS RATE, Fp (INCH/HR) = 0.74
SUBAREA AVERAGE PVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA (ACRES) = 25.40 SUBAREA RUNOFF (CFS) = 64.04
EFFECTIVE AREA (ACRES) = 54.10 AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA (ACRES) = 54.1 PEAK FLOW RATE (CFS) = 136.39

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	142.42	13.88	3.249	0.74 (0.07)	0.10	49.8	21.00
2	136.39	17.02	2.875	0.74 (0.07)	0.10	54.1	18.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE (CFS) = 142.42 Tc (MIN.) = 13.88
AREA-AVERAGED Fm (INCH/HR) = 0.07 AREA-AVERAGED Fp (INCH/HR) = 0.74
AREA-AVERAGED Ap = 0.10 EFFECTIVE AREA (ACRES) = 49.84

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 54.1 TC (MIN.) = 13.88
EFFECTIVE AREA (ACRES) = 49.84 AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.100
PEAK FLOW RATE (CFS) = 142.42

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	142.42	13.88	3.249	0.74 (0.07)	0.10	49.8	21.00
2	136.39	17.02	2.875	0.74 (0.07)	0.10	54.1	18.00

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END OF RATIONAL METHOD ANALYSIS