12.0 APPENDICES

APPENDIX A LEGAL DESCRIPTION

APPENDIX B TRAFFIC ACCESS ANALYSIS

APPENDIX C POLICE SECURITY STANDARDS

Page 9 • NEW DEFINITION

11. <u>Individual Property Developer(s)</u>: shall refer to the Kontos Enterprises property located at the southeast corner of the Archibald Center Specific Plan, their successor or their agent. This definition shall also refer to any other individual property developer(s) in the Support Commercial Zone.

Page 25 • Paragraph 4

3.3 LAND USE PLAN

......The small portion of the site in this category (3.9 acres) will provide for commercial use that......

Page 26 • Table

LAND USE SUMMARY

Land Use Category	Approximate Acreage	Percent Acreage	Building Numbers
Business Park	10.9	37.2%	1-17
Bulk Warehouse Retail	14.5	49.6%	18-20
Support Commercial	3.9	13.2%	21-25
Total Site Area	29.3 Acres	100%	

Interior public streets will occupy approximately 1.8 additional acres.

3.4.3 SUPPORT COMMERCIAL CATEGORY

The Support Commercial Category includes approximately 3.9 acres and is......

Page 35 • Paragraph 2

3.4.3.2 Conditionally Permitted Uses

*Remove "Liquor Store" from 3.4.3.2 and add it to:

3.4.3.3 Prohibited Uses

Liquor Store

Page 82 • Table

3.5.5.2 Minimum Building and Parking Area Setbacks

	Parking	Building
Archibald Avenue	13'	45'
Philadelphia Street	20'	45'
Local Street	10'	20'
Pomona Freeway	5'	15'
Cucamonga Creek Channel	5'	5'
Interior Property Line	5'	None
	(continued)	

Rear Property Line

The Kontos Enterprises property, which lies directly to the southeast of the Archibald Center Specific Plan, is herein included in the Archibald Center Specific Plan and shall have a building setback of thirty-five (35) feet on Archibald Avenue.

Page 83 • Paragraph 3

3.5.5.5 Minimum Parking Requirements

• The minimum stall width for standard spaces shall be nine (9) feet.

Page 90 • Paragraph 2

3.5.6.7 Permanent Freestanding Building Identification (Monument) Signs

Any parcel in the Support Commercial zone that is physically adjacent to the right-of-way of the Pomona 60 State Freeway shall be allowed a freestanding sign which shall not exceed thirty-five (35') feet in height if the adjacent freeway segment is at or below the grade of the site on which the sign is located or shall not exceed forty-five (45') in height if the adjacent freeway segment is above the grade of the site, and shall be subject to the following limitations:

- The area of a freeway oriented sign shall not exceed 150 square feet on any display surface.
- Any advertisement text, symbols, or other indications displayed on the sign face shall be limited to not more than five (5) words, letters numbers figures symbols, or other indications used as a substitute for words.
- No vertical or horizontal dimension of the display surface shall exceed twenty (20') feet.

Page 90 • Paragraph 3

3.5.6.8 Permanent Vehicular Directional Signs

The signs may be illuminated.

Page 111 • Paragraph 1

4.2.1 POMONA FREEWAY

The Pomona Freeway Edge consists of two components. The first, a five (5) foot wide landscape strip for the Support Commercial and a ten (10) foot wide landscape strip for the Bulk Wharehouse Retail, is outside of.......

Page 116 • Paragraph 7• NEW LAST PARAGRAPH

4.3.1 GENERAL GUIDELINES

The Individual Property Developer(s) shall not be limited to only the plant materials shown on the plant palette and will be subject to review by the City of Ontario's Public Facilities plan check section.

Page 144 • NEW LAST PARAGRAPH

10.0 DEVELOPMENT PHASING

Individual Property Developers are not considered a part of this section.

13.0 APPENDICES

APPENDIX A LEGAL DESCRIPTION

APPENDIX B TRAFFIC ACCESS ANALYSIS

APPENDIX C POLICE SECURITY STANDARDS

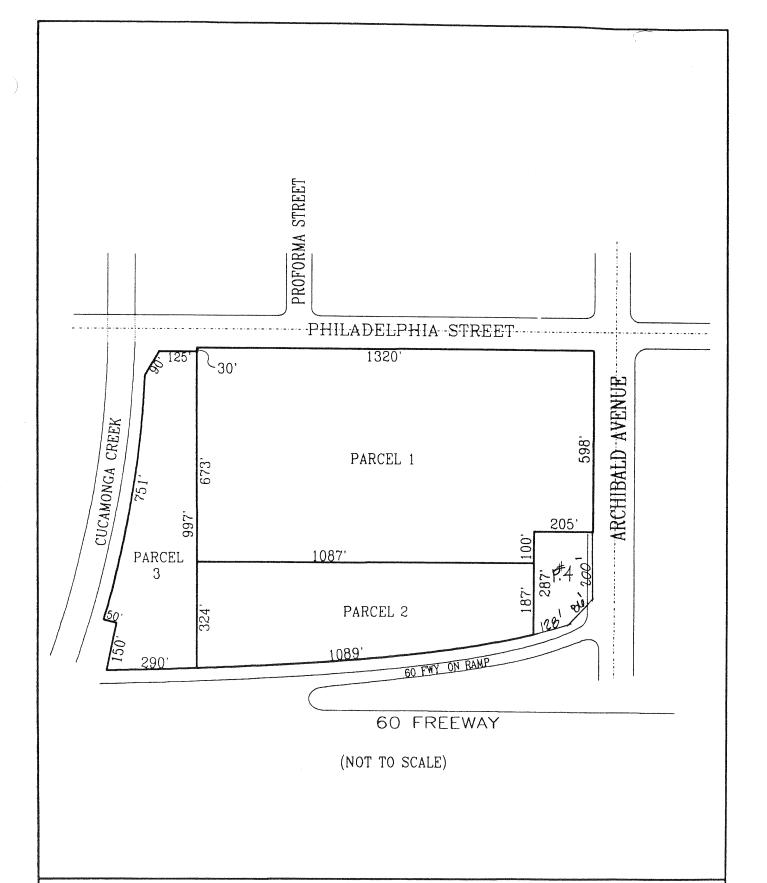
LEGAL DESCRIPTION:

PARCEL NO. 4:

THE NORTHWEST QUADRANT OF ROUTE 60 AND ARCHIBALD AVENUE IN ONTARIO, COUNTY OF SAN BERNADINO, STATE OF CALIFORNIA.

PARCEL NUMBER 1 OF PARCEL MAP NO. 139, AS PER PLAT RECORDED IN BOOK 2 OF PARCEL MAPS, PAGE 43, RECORDS OF SAID COUNTY.

EXCEPTING THEREFROM THAT PORTION CONVEYED TO THE STATE OF CALIFORNIA BY DEED RECORDED MAY 15, 1969 IN BOOK 7232, PAGE 585, OFFICIAL RECORDS.





ARCHIBALD CENTER SPECIFIC PLAN
ONTARIO, CALIFORNIA



TRAFFIC STUDY REPORT ONTARIO HOME FURNISHING CENTER Ontario, California

Prepared For:

SDC DEVELOPMENT 1601 Avocado Newport Beach, CA 92660

Prepared By:

LINSCOTT, LAW & GREENSPAN, ENGINEERS
1580 Corporate Drive
Suite 122
Costa Mesa, California 92626

July, 1990

2-901420-1

LINSCOTT, LAW & GREENSPAN, ENGINEERS TRANSPORTATION PLANNING • TRAFFIC ENGINEERING • PARKING

1580 CORPORATE DRIVE, SUITE 122, COSTA MESA, CALIFORNIA 92626 • (714) 641-1587

July 3, 1990

PHILIP M. LINSCOTT, P.E. JACK M. GREENSPAN, P.E. WILLIAM A. LAW, P.E. PAUL W. WILKINSON, P.E. LEON D. WARD, P.E. DONALD W. BARKER, P.E.

Mr. Steven A. Lichtenberger SDC DEVELOPMENT 1601 Avocado Newport Beach, CA 92660

Subject: TRAFFIC IMPACT ANALYSIS

ONTARIO HOME FURNISHINGS CENTER

Ontario, California

Dear Steven:

Pursuant to your authorization, we are pleased to submit this Traffic Study Report for the Ontario Home Furnishing Center located northwest of the Pomona Freeway and Archibald Avenue in Ontario.

The report addresses the potential traffic impacts associated with the industrial/freeway showroom project in a near-term (1995) and buildout (2010) cumulative traffic setting. A summary of our findings and recommendations is located on page 17 of the report.

Linscott, Law & Greenspan has welcomed the opportunity to provide this analysis and are prepared to provide additional consultation as may be required. Please feel free to call if you have any questions or need further assistance.

Very truly yours,

LINSCOTT, LAW & GREENSPAN, ENGINEERS

Jay L. Nelson

Transportation Engineer II

JLN/1420-1

Submittal:

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Linscott, Law & Greenspan, Engineers

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EXHIBIT	DESCRIPTION PAGE NUMBER
1	VICINITY MAP 2
2	SITE PLAN 3
3	PM PEAK HOUR PROJECT TRAFFIC 7
4	1995 PM PEAK HOUR TRAFFIC WITHOUT PROJECT 9
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INTRODUCTION

This report evaluates the potential traffic impacts associated with the proposed Ontario Home Furnishing Center. The planned industrial/freeway showroom project is located north of the Pomona Freeway (SR-60) and south of Philadelphia Street, between Archibald Avenue and the Cucamonga Creek Channel in Ontario. analysis evaluates the near-term 1995 and buildout (2010) traffic conditions during the critical PM peak hour at key intersections with and without the proposed project development. The access opportunities and constraints for the freeway showroom and other support commercial uses were evaluated in a prior letter report completed by Linscott, Law and Greenspan, dated March 9, 1990. The prior analysis included preliminary schematic street plans to illustrate recommended access locations and potential striping and median layout along the freeway showroom and support commercial project frontage.

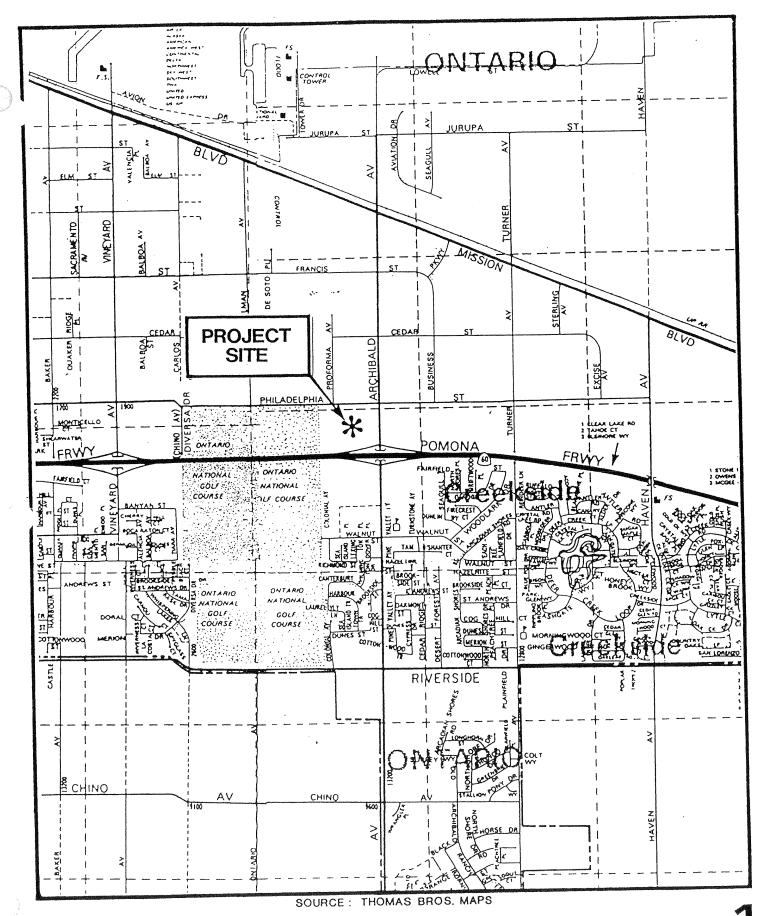
PROJECT DESCRIPTION AND LOCATION

The project is located on a 28 acre site, and will include light industrial, freeway showroom, and support commercial uses. General light industrial uses with a total building area of 157,082 square-feet are planned on the northwest portion of the site. The remainder of the project includes 206,091 square-feet of freeway showroom space, two fast-food restaurants with a combined building area of approximately 8,000 square-feet, and a service station.

The project location and surrounding street system is presented in Exhibit 1. Access to the project will be provided from Archibald Avenue and Philadelphia Street. Access to the Pomona Freeway is provided by a diamond interchange adjacent to the project on Archibald and west of the project at Vineyard.

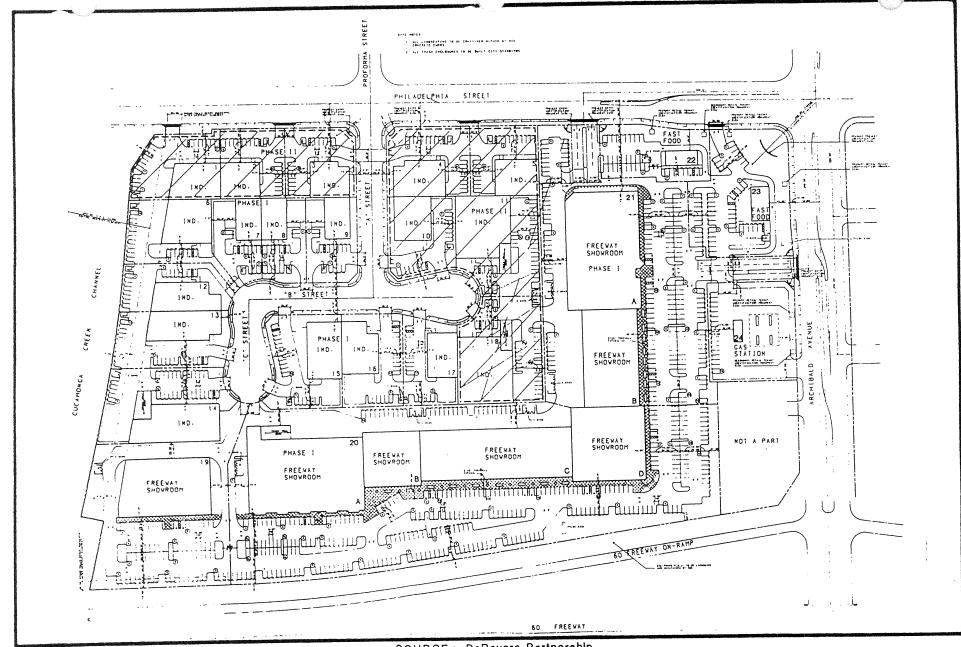
The site plan for the project is illustrated in Exhibit 2. For the showroom and support commercial portion of the project two driveways are planned on both Archibald Avenue and Philadelphia Street, at the locations recommended in the prior traffic access analysis for the project.

The main project driveway on Archibald is located 365 feet south of Philadelphia (centerline to centerline) and would provide left- and right-turn ingress, but the raised median would be constructed to prohibit left-turn egress from the project onto Archibald. A second driveway on Archibald would be located 220 feet south of the major driveway and would be restricted to right-turn access only. Access to the World Oil Parcel (labeled as not a part on the site plan) is not considered in this analysis.



NORTH

VICINITY MAP ONTARIO HOME FURNISHING CENTER



SOURCE: DeRevere Partnership



SITE PLAN ONTARIO HOME FURNISHING CENTER

On Philadelphia a full access driveway will be located 508 feet west of Archibald (centerline to centerline). A second driveway will be restricted to right-turn access only and will be located about 245 feet west of Archibald. Additional access will be provided via the cul-de-sac planned in the industrial portion of the project. This access would primarily be used by service vehicles and employees.

A new cul-de-sac is proposed opposite Proforma Street as the major access for the industrial component of the project. As shown on the site plan, three additional driveways are proposed on Philadelphia to access the industrial buildings.

TRAFFIC FORECASTING AND IMPACT EVALUATION METHODOLOGY

In order to estimate the traffic impact characteristics of the project, a multi-step process has been utilized. The first step is traffic generation, which estimates the total arriving and departing traffic at the site on a peak hour and daily basis. The traffic generation potential of the site is estimated by applying the appropriate trip generation rates for each of the proposed land uses.

The second step of the evaluation process is traffic distribution which identifies the origins and destinations of inbound and outbound project traffic. These origins and destinations are based on available travel routes and the general demographics of the area.

The third step is traffic assignment, which involves the allocation of project traffic estimates to area streets and intersections. Traffic assignment is typically based on minimization of travel time which may or may not involve the shortest route, depending on prevailing operating conditions and travel speeds. Traffic approach distribution patterns are indicated by general percentage orientation, while traffic assignment is based on specific volume forecasts related to development conditions.

With the forecasting process complete and project traffic assignments developed, the impact of the project is analyzed by comparing the operational conditions at the intersections adjacent to the project for near term (1995) and buildout (2010) scenarios both with and without anticipated project traffic.

TRAFFIC GENERATION FORECAST

Traffic generation is expressed in terms of vehicle trip ends (TE) where a trip end is a one-way vehicular movement either entering or departing the study site. Generation factors for retail and industrial land uses are typically developed based upon the number of trip ends per 1,000 square feet of gross floor

area (TE/1,000 SF). The forecast is accomplished by multiplying the floor area (in thousands of square-feet) by the appropriate generation factors.

Traditional sources for traffic generation factors include <u>Trip Generation</u>: <u>An Informational Report</u> published by the Institute of Transportation Engineers (ITE), various <u>Progress Reports on Trip Ends Generation Research Counts</u> by Caltrans, and published or unpublished in-house studies by other transportation agencies and professionals. For this analysis trip generation rates from the 4th Edition of <u>Trip Generation</u>, published by ITE were used.

Table 1 summarizes the trip generation rates, and presents the forecasted project traffic. As shown in Table 1, the project is expected to generate 7,800 trips on a daily basis (one half arriving, one half departing), with 535 trips anticipated during the PM peak hour (210 inbound, 325 outbound).

Most of the showroom space planned for the center is expected to open after the typical morning peak period which occurs between 7:00 and 9:00 AM. Therefore, only the trip generation forecast for the evening peak hour has been completed for the project.

A significant portion of the trips associated with the fast food restaurants and the service station are not new trips, but represent vehicles already on the street that will merely stop off at the project as they pass by. Assuming 50 percent of the trips to the fast food and service station are vehicles passing by on their way to another destination a total of 145 PM peak hour project trips would be existing pass-by traffic. However, in this analysis the project traffic has not been reduced for pass-by traffic and therefore depicts a "worst-case" condition.

TRAFFIC DISTRIBUTION AND ASSIGNMENT

The general distribution of project traffic is based on anticipated travel patterns in the area. Approximately 40 percent of the project traffic is expected to be oriented to and from the Pomona Freeway at Archibald, with twenty percent of the project traffic distributed each direction on the freeway. The remaining project traffic was evenly distributed in the four compass directions on Archibald Avenue and Philadelphia Street.

The anticipated PM peak hour project traffic volumes at each of the proposed driveways and at key intersections are presented in Exhibit 3. These volumes were estimated by applying the distribution pattern discussed above to the PM peak hour traffic forecast in Table 1.

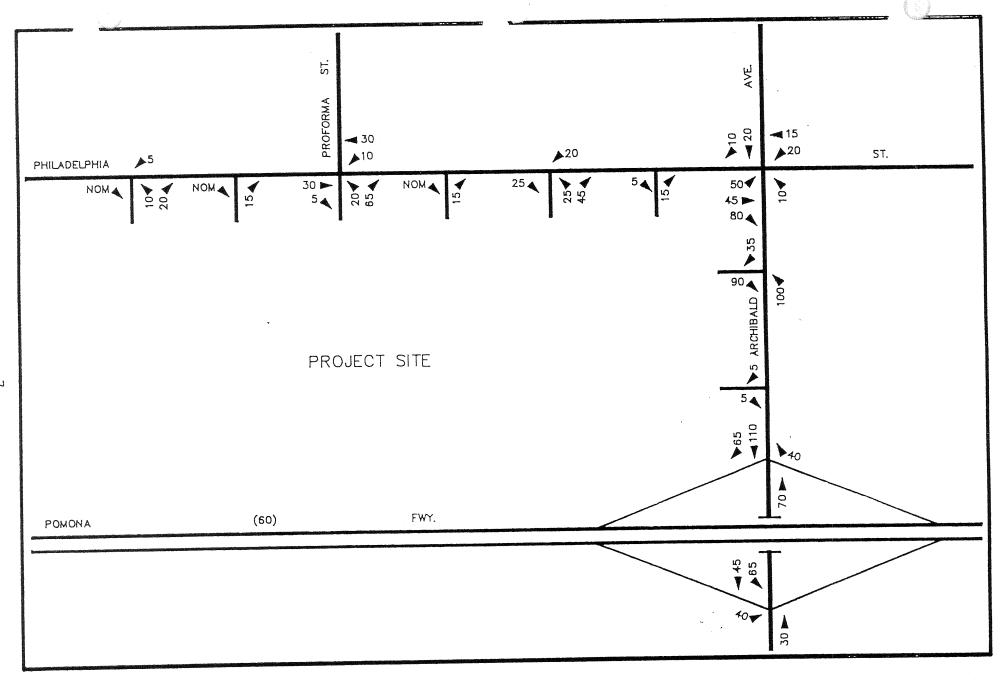
TABLE 1

TRAFFIC GENERATION FORECAST
Ontario Home Furnishing Center

	P M INBOUNI	PEAK H		DAILY 2-WAY
GENERATION FACTORS ¹				
General Light Industrial (TE/TSF)	0.13	0.91	1.04	6.97
Freeway Showroom (TE/TSF)	0.20	0.19	0.39	4.35
Fast Food Restaurant (TE/TSF)	17.11	16.15	33.26	632.13
Service Station (TE/Station)	13.00	12.00	25.00	748.00
GENERATION FORECAST ²				
General Light Industrial (157,082 SF)	· 20	145	165	1,090
Freeway Showroom (206,091 SF)	40	40	80	900
Fast Food Restaurant (8,000 SF)	135	130	265	5,060
Service Station	· <u>15</u>	<u>10</u>		<u>750</u>
TOTAL	210	325	535	7,800

^{1.} Source: Institute of Transportation Engineers, Trip Generation, 4th Edition, 1987. Furniture Store trip generation rates (land use 890) were used for the Freeway Showroom.

^{2.} Forecasts are rounded to the nearest 5 vehicles on a peak hour basis and to the nearest 10 vehicles on a daily basis.





7

FUTURE 1995 AND 2010 PM PEAK HOUR TRAFFIC VOLUMES

Future 1995 and 2010 PM peak hour traffic volumes for the three key intersections on Archibald were received from Gary Cohoe, at the City of Ontario. The volumes were taken from the <u>Haven Avenue Interchange at Route 60, Traffic Analysis Study</u> completed by Mohle, Grover & Associates. The future traffic volumes were derived by applying a growth rate to the existing traffic volumes to account for development outside of the study area. Then, traffic assignments related to specific developments were added to the background traffic volumes to incorporate planned and future development in the area. A growth rate of ten percent was used for 1995 forecast and thirty percent was applied for the 2010 analysis.

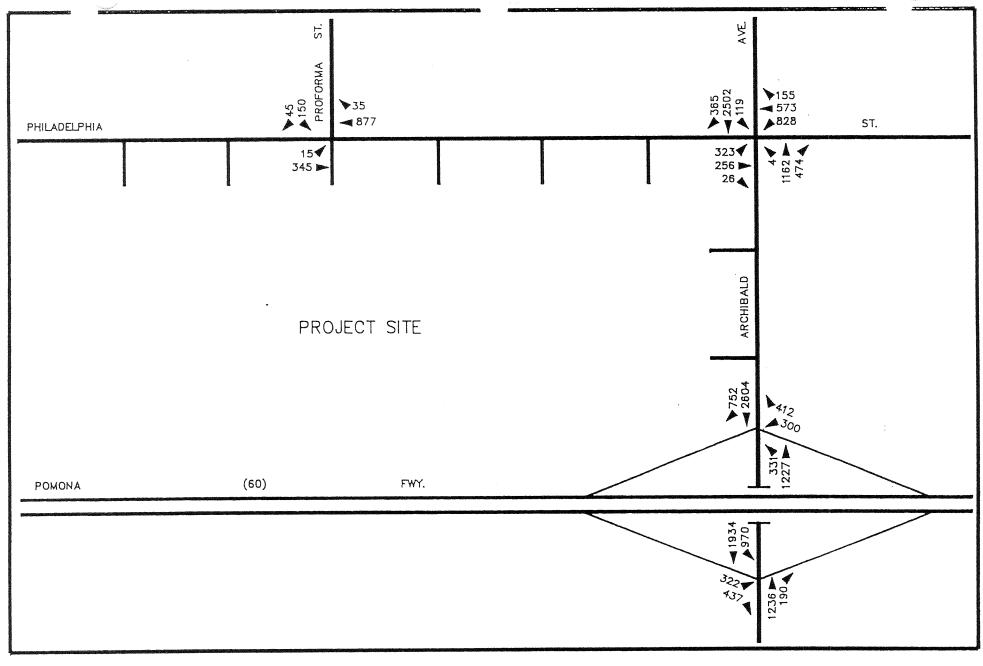
The 1995 and 2010 traffic forecasts completed by Mohle, Grover & Associates assumed light industrial development would occur on the entire proposed Ontario Home Furnishing site and that access to the site would only be provided on Philadelphia Street. Therefore, these future traffic volumes were adjusted to remove the prior traffic forecast for the site to obtain a base 1995 and 2010 traffic condition without any project traffic. The volumes to and from Proforma Street at Philadelphia Street were obtained from the traffic analysis for the Birk Project located north of Philadelphia. The through volumes on Philadelphia at Proforma were calculated from the traffic volumes leaving and approaching the Philadelphia/Archibald intersection.

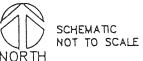
The 1995 and 2010 PM peak hour traffic volumes without the project are presented in Exhibits 4 and 5, respectively. The PM peak hour project traffic volumes illustrated in Exhibit 3 were then added to the baseline 1995 and 2010 volumes to obtain the 1995 and 2010 PM peak hour traffic volumes with the proposed project. These volumes are shown in Exhibits 6 and 7.

PEAK HOUR INTERSECTION ANALYSIS

The impact of the project has been evaluated for the critical PM peak hour using the Intersection Capacity Utilization (ICU) method at the Archibald/SR-60 Freeway Ramps, Archibald/Philadelphia, and Philadelphia/Proforma intersections. The impact of the proposed project was determined by comparing the future 1995 and 2010 conditions at these locations with and without the anticipated project traffic.

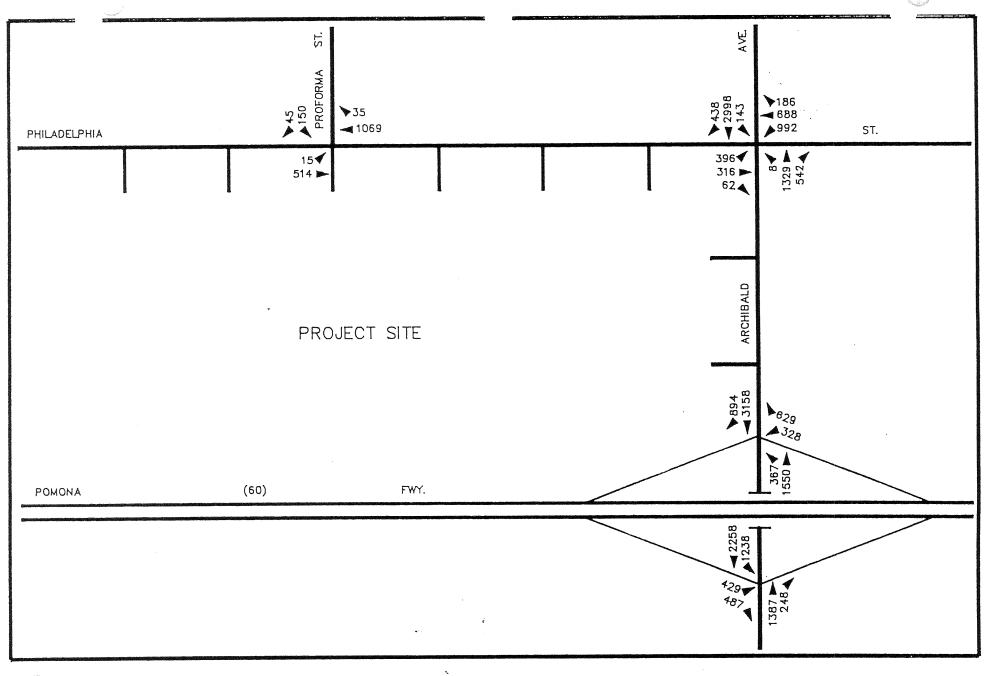
The ICU procedure assumes the traffic flow characteristics of a signalized intersection and computes Level of Service (LOS) for the total intersection based upon a summation of volume to capacity (v/c) ratios for key conflicting movements. The ICU numerical value represents the percent of the signal green time, and thus capacity, required by existing or future traffic.





1995 PM PEAK HOUR TRAFFIC WITHOUT PROJECT

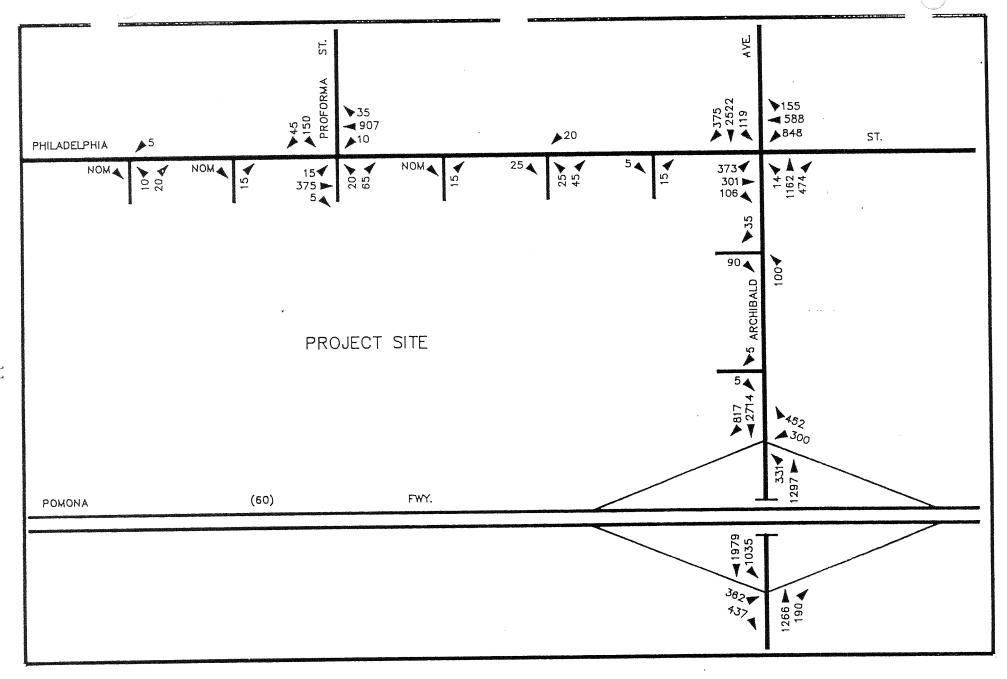
ONTARIO HOME DIPHICHINO CENTER





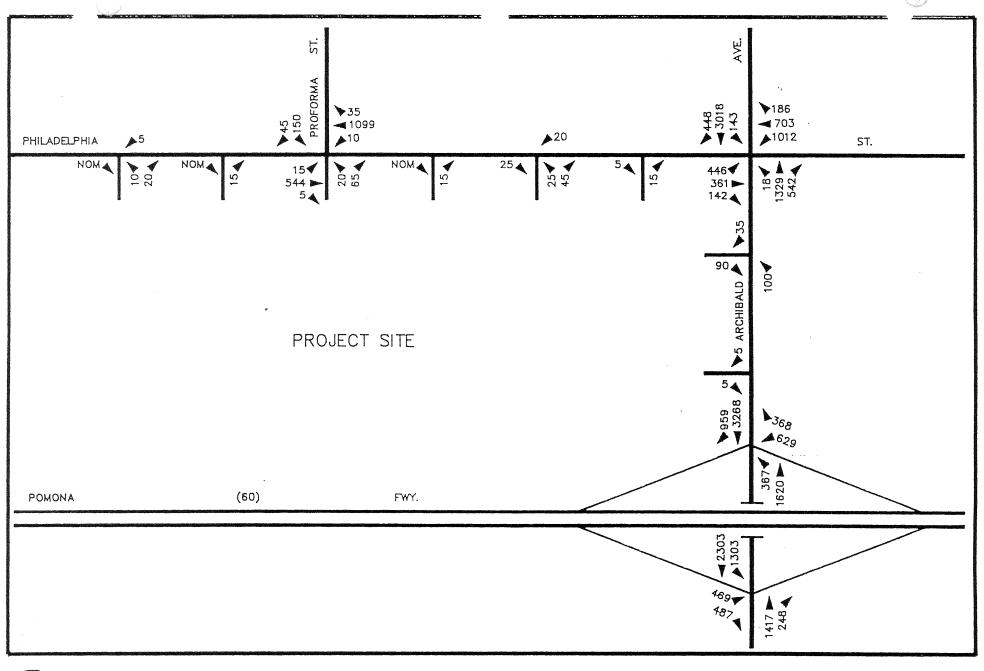
2010 PM PEAK HOUR TRAFFIC WITHOUT PROJECT

2





1995 PM PEAK HOUR TRAFFIC WITH PROJECT





2010 PM PEAK HOUR
TRAFFIC WITH PROJECT

The ICU translates to a Level of Service which is a relative measure of driver satisfaction. Six Levels of Service have been defined ranging from A (ICU of 0.60 or less, representing free flow with little congestion) to F (ICU over 1.00, representing forced flow with significant congestion). Level of Service D (ICU of 0.81 to 0.90), is traditionally considered the maximum acceptable level for urban and suburban peak hour conditions. At Level D, most traffic clears on the first available green phase, but short vehicle queues may occur. Average vehicle speeds are on the order of 20 to 25 miles per hour including stops. Level of Service E is characterized by long queues of waiting vehicles which exist over extended periods of time often blocking nearby intersections and requiring several cycles to clear.

The capacity analysis is based on the planned intersection configurations indicated in prior traffic studies. The planned lane configurations at the four key intersections evaluated in this study are illustrated in Exhibit 8.

Table 2 presents the ICU/LOS values at the key intersections. The computer-generated ICU calculations are presented at the end of the report. The four following scenarios were evaluated for each intersection:

- o 1995 Conditions Without Project Traffic
- o 1995 Conditions With Project Traffic
- o 2010 Conditions Without Project Traffic
- o 2010 Conditions With Project Traffic
- o 2010 Conditions With Project & 10% TDM Reduction

As shown in Table 2, all of the key intersections will operate at an acceptable Level of Service (LOS D or better) in 1995 with the completion and full occupancy of the project. The addition of forecasted project traffic is expected to increase the ICU value by 0.02 or 0.03 at the three key intersections for both the near term (1995) and buildout (2010) scenarios. Further, the increase in the ICU value would be smaller if the project traffic was reduced to account for pass-by traffic at the site.

At buildout, which includes more extensive area development and an additional twenty percent increase in existing traffic, LOS E is forecast at the Archibald/Philadelphia intersection, and LOS D is anticipated at the Pomona Freeway ramps on Archibald. The addition of project-related traffic to the baseline 2010 traffic volumes are not expected to change the level of service at any of the key intersections.

Transportation demand management (TDM) programs, required as a result of the South Coast Air Quality Management District's (SCAQMD) Regulation XV, are expected to significantly reduce the buildout 2010 traffic volumes. Regulation XV requires the preparation and implementation of a commute assistance program

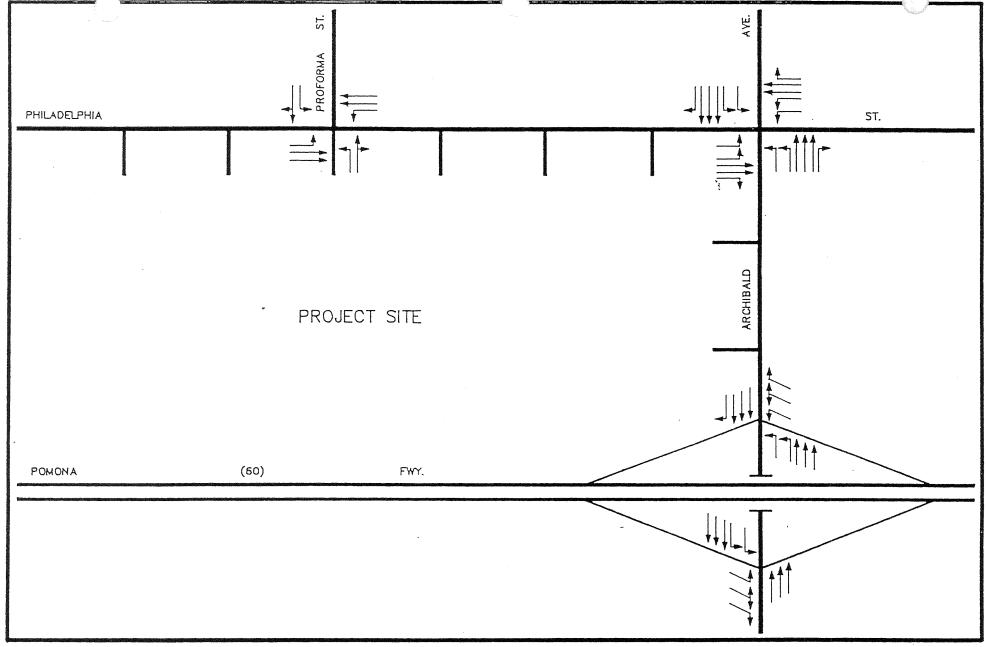




TABLE 2

PM PEAK HOUR LEVEL OF SERVICE SUMMARY

Ontario Home Furnishing Center

	and an arrangement of collections about 1 to 12 to		ICU - LOS¹		
LOCATION	1995 WITHOUT PROJECT	1995 WITH PROJECT	2010 WITHOUT PROJECT	2010 WITH PROJECT	2010 WITH 10% TDM RED.
Archibald Avenue/ Philadelphia Street	.80/C	.82/D	.95/E	.98/E	.89/D
Archibald Avenue/ WB SR-60 Ramp	(.77/C)² .68/B	(.80/C)² .71/C	.83/D	.85/D	.78/C
Archibald Avenue/ EB SR-60 Ramp	.67/B	.70/B	.81/D	.84/D	.76/C
Philadelphia Street/ Proforma Street	.38/A	.44/A	.43/A	.49/A	.45/A

- 1. Intersection Capacity Utilization/Level of Service, see appendix for an explanation of the ICU/LOS concept and detailed calculations.
- 2. This ICU value assumes only a single northbound left-turn lane, the other ICU values at this intersection assume two northbound left-turn lanes, as indicated in prior traffic studies.

designed to achieve an Average Vehicle Ridership (AVR) of 1.5 people per vehicle. A conservative estimate of the traffic reduction impacts of regulation XV are also summarized Table 2. TDM programs can reduce traffic volumes by as much as 30 percent. A 10 percent reduction in the buildout 2010 traffic volumes would result in level of service D or better at each of the intersections evaluated in this report.

SITE ACCESS

The location of the freeway showroom and support commercial driveways were evaluated in the traffic access analysis for the project completed in March, and have not been modified. A raised median is planned on Archibald that will permit right-turn-only access at the minor driveway and prohibit the left-turn exit from the site at the major driveway. The 200-foot left-turn pocket proposed at the major driveway on Archibald is expected to provide sufficient storage for the anticipated left-turn volumes into the site. The proposed left-turn lane on Archibald into the project will provide sufficient storage for eight vehicles and an average of less than three vehicles per cycle are anticipated during the PM peak hour.

The number and length of gaps in the through southbound traffic stream on Archibald were evaluated to determine if sufficient gaps were available for traffic to make a left turn from Archibald into Ontario Home Furnishing Center. Based on the Passer II analysis (included in the appendix) the traffic signal timing at intersections on Archibald adjacent to the project were calculated using 100 second cycle lengths. In order to conservatively evaluate left-turn access to the project from Archibald, the 2010 PM peak hour traffic volumes without any reduction for TDM were used in this analysis.

The northbound left-turn phase at Archibald and Philadelphia is expected to create a 10 second gap in the southbound traffic stream during each 100 second cycle. Further, the traffic signal is expected to create additional gaps when traffic on Archibald is stopped to allow traffic on Philadelphia to pass through the intersection. Breaks in the southbound traffic stream on Archibald totaling approximately 19 seconds each cycle are expected to provide adequate gaps for anticipated project traffic to safely make a left-turn from Archibald into the Ontario Home Furnishing site.

TRAFFIC SIGNAL WARRANT ANALYSIS

A signal warrant analysis was performed at the Philadelphia/ Proforma intersection based on Caltrans estimated average daily traffic volumes. Near term 1995 daily traffic volumes were projected from the PM peak hour volumes shown in Exhibit 6 and were used in the signal warrant analysis. The traffic signal warrant sheet can be found following the ICU calculations at the end of Traffic signal warrants are not met based on the anticipated project traffic volumes at the proposed cul-de-sac which will become the south leg of the intersection. Further, the warrants would not be satisfied even if the proposed cul-desac was the only access to the industrial portion of the project. The potential traffic from the development north of Philadelphia is significantly greater than the traffic anticipated from the Ontario Home Furnishing project. However, based on 1995 volumes neither the minimum vehicular warrant or the interruption of continuous traffic warrant are satisfied at the Philadelphia/ Therefore we do not recommend that the Proforma intersection. intersection be signalized until additional analysis indicates that a signal is required.

SUMMARY AND CONCLUSIONS

- The proposed Ontario Home Furnishing Center includes 206,091 square-feet of freeway showroom space, two fast food restaurants, and a service station. General light industrial uses with a total building area of 157,082 square-feet are planned on the northwest portion of the site.
- o The project is expected to generate 7,800 trips on a daily basis (one half arriving, one half departing), with 535 trips anticipated during the PM peak hour (210 inbound, 325 outbound).
- o At the completion and full occupancy of the project the adjacent intersections are expected to operate at level of service D or better during the PM peak hour.
- o At buildout (2010) the Philadelphia/Archibald intersection is expected to operate at LOS E both with or without the proposed project if no traffic reduction is assumed for transportation demand management (TDM) programs. With a ten percent reduction in traffic expected as a result of required TDM programs LOS D is calculated at the intersection. The other key intersections are expected to operate at LOS D or better without assuming any reduction in traffic associated with TDM and LOS C or better with TDM (see Table 2).
- o The anticipated project traffic is not expected to change the buildout 2010 level of service at any of the adjacent intersections during the critical PM peak hour.
- o Traffic signals are not warranted at any of the project driveways, including the Philadelphia/Proforma intersection.

Linscott, Law & Greenspan, Engineers

o The proposed 200-foot left-turn lane on Archibald at the major project driveway is designed to provide sufficient vehicular storage for traffic entering the site.

APPENDIX A

LEVEL OF SERVICE (LOS) AND INTERSECTION CAPACITY UTILIZATION (ICU)

Level of Service is a term used to describe prevailing conditions and their effect on traffic. Broadly interpreted, the Level of Service concept denotes any one of a number of various traffic volumes. Level of Service is a qualitative measure of the effect of such factors as travel speed, travel time, interruptions, freedom to maneuver, safety, driving comfort and convenience.

Six Levels of Service, A through F, have been defined in the Highway Capacity Manual of 1985. Level of Service A describes a condition of free flow, with low traffic volumes and relatively high speeds, while Level of Service F describes forced traffic flow at low speeds with jammed conditions and queues which cannot clear during the green phases.

The Intersection Capacity Utilization (ICU) method of intersection capacity analysis has been used in our studies. It directly relates traffic demand and available capacity for key intersection movements, regardless of present signal timing. The capacity per hour of green time for each approach is calculated based on the methods of the Highway Capacity Manual. The proportion of total signal time needed by each key movement is determined and compared to the total time available (100 percent of the hour). The result of summing the requirements of the conflicting key movements plus an allowance for clearance times is expressed as a decimal fraction. Conflicting key traffic movements are those opposing movements whose combined green time requirements are greatest.

The resulting ICU represents the proportion of the total hour required to accommodate intersection demand volumes if the key conflicting traffic movements are operating at capacity. Other movements may be operating near capacity, or may be operating at significantly better levels. The ICU may be translated to a Level of Service as tabulated below.

The Levels of Service (abbreviated from the Highway Capacity Manual) are listed here with their corresponding ICU and Load Factor equivalents. Load Factor is that proportion of the signal cycles during the peak hour which are fully loaded; i.e., when all of the vehicles waiting at the beginning of green are not able to clear on that green phase.

LEVEL OF SERVICE	LOAD FACTOR	EQUIVALENT
A (free flow) B (rural design) C (urban design) D (maximum urban design) E (capacity) F (forced flow)	0.0 0.0 - 0.1 0.1 - 0.3 0.3 - 0.7 0.7 - 1.0 Not Applicable	0.0 - 0.60 0.61 - 0.70 0.71 - 0.80 0.81 - 0.90 0.91 - 1.00 Not Applicable

SERVICE LEVEL A

There are no loaded cycles and few are even close to loaded at this service level. No approach phase is fully utilized by traffic and no vehicle waits longer than one redindication.

SERVICE LEVEL B

This level represents stable operation where an occasional approach phase is fully utilized and a substantial number are approaching full use. Hany drivers begin to feel restricted within platoons of vehicles.

SERVICE LEVEL C

At this level stable operation continues. Loading is still intermittent but more frequent that at Level B. Occasionally drivers may have to wait through more than one red signal indication and backups may develop behind turning vehicles. Most drivers feel somewhat restricted, but no objectionably so.

SERVICE LEVEL D

This level encompasses a zone of increasing restriction approaching instability at the intersection. Delays to approaching vehicles may be substantial during short peaks within the peak hour, but enough cycles with lower demand occur to permit periodic clearance of queues, thus preventing excessive backups. Drivers frequently have to wait through more than one red signal. This level is the lower limit of acceptable operation to most drivers.

ERVICE LEVEL E

This represents near capacity and capacity operation. At capacity (ICU = 1.0) it assents the most vehicles that the particular intersection can accommodate. However, full unization of every signal cycle is seldom attained no matter how great the demand. At this level all drivers wait through more than one red signal, and frequently through several.

SERVICE LEVEL F

Jammed conditions. Traffic backed up from a downstream location on one of the streets restricts or prevents movement of traffic through the intersection under consideration.

TABLE <u>IA</u>

VOLUME-CAPACITY ANALYSIS

PHILADELPHIA STREET & ARCHIBALD AVENUE

PM

	1995 C (Haven/	SR-60	Study)	1995 CONDITION WITHOUT PROJECT				PLUS PROJECT TRAPFIC				WITH 10% TDM REDUCTION											
TKBKBVOK	AOPAKE	CAP	V/C RATIO		TOTAL VOLUKE	CAP	V/C RATIO	VOL.	TOTAL VOLUME		V/C RATIO	VOL.	TOTAL VOLUMB	CAP	V/C RATIO		TOTAL VOLUME	CAP	V/C RATIO		TOTAL VOLUME	СЛР	V/C RATIO
NBL NBT NBR	29 1162 474	5700	0.05 * 0.20 0.28	- 25 0 0	1162	3400 5700 1700	0.05 [*] 0.20 0.28	10 0 0	1162	5700	0.05 * 0.20 0.28	-1 -116 -47	1046	3400 5700 1700	0.18	0 0 0	0	0	0.00 0.00 0.00	. 0 0	0	0	0.00 0.00 0.00
SBL SBT SBR	119 2502 370	5700		0 0 -5	2502	5700	0.05 0.44 * 0.21	0 20 10		3400 5700 1700	0.05 0.44 * 0.22	-12 -252 -38	2270	3400 5700 1700	0.40 *	0 0 0	0	0	0.00 0.00 0.00	0 0 0	0	(0.00 0.00 0.00
O EBL EBT EBR	368 301 181	3400 3800 1700	0.11 0.08 * 0.11	-45 -45 -155	256	3800	0.10 0.07 * 0.05	50 45 75	301	3800		-37 -30 -11	271	3400 3800 1700	0.10 0.07 * 0.05	0 0 0	0	0	0.00 0.00 0.00	0 0 0	0	(0.00 0.00 0.00
ABE ABE	828 578 155	3800	0.24 ± 0.15 0.09	0 - <u>5</u> 0	573	3400 3800 1700	0.15	20 15 0	588	3400 3800 1700		-85 -59 -16	529	3400 3800 1700		0 0 0	0	0	0.00 0.00 0.00	0 0 0) 0		0.00 0.00 0.00
	CLEARANCI		0.00 ==== 0.81		CLEARANG		0.00 ==== 0.80		CPEYKYN		0.00 ==== 0.82		CLEARAN		0.00 ==== 0.74		ICU VAL		0.00 ==== 0.00		ICA AYP		0.00 ==== 0.00
!	LEVEL OF	SERVI	 C E = D		PEAEP 0	r serv	ICE= C		PEAET 0	F SERV	ICE= D		LEVEL O	F SERV			PSASP 0	F SERV			PEAEP 0	r ser	VICE=

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λ:1420N1P.ICU

TABLE B VOLUME-CAPACITY ANALYSIS PHILADELPHIA STREET & ARCHIBALD AVENUE PM

-6	NDITIC R-60 S	Study)		WITHOUT				PLUS PR TRA	OJECT FPIC	~~~~		WITH 10 REDU	₹ TDM CTION									
	CAP	V/C RATIO		TOTAL	СУБ	V/C RATIO		TOTAL	CAP	V/C RATIO		TOTAL VOLUKE	СЛР	V/C RATIO		TOTAL VOLUME	СХР	V/C RATIO		TOTAL VOLUME	CAP	V/C RATI
		0.05 *	-25	8	3400	0.05 ±	10	18	3400	0.05 ±	-2	16	3400	0.05 *	0	0	0	0.00	0	0	(0.00
		0.23	0		5700	0.23	0	1329	5700	0.23	-133	1196	5700	0.21	0	0	0	0.00	0	0	0	0.00
	1700		0		1700	0.32	0	542	1700	0.32	-54	488	1700	0.29	0	0	0	0.00	0	0	0	0.00
4 N	3400	0.05	0	143	3400	0.05	0	143	3400	0.05	-14	129	3400	0.05	0	0	0	0.00	0	0	(0.00
		0.53 *	•		5700	0.53 *	20	3018	5700	0.53 ±	-302	2716	5700	0.48 *	0	0	0	0.00	0	0	(0.00
	1700		-5			0.26	10	448	1700	0.26	-45	403	1700	0.24	0	0	0	0.00	0	0	(0.00
ıο	3400	0.13	-45	396	3400	0.12	50	446	3400	0.13	- 45	401	3400	0.12	0	. 0	0	0.00	0	0	(0.00
		0.10 4	-45		3800	0.08 *	45	361	3800	0.10 ±	-36	325	3800	0.09 *	0	0	0	0.00	0	0	(0.00
		0.13	-155			0.05	75	137	1700	0.08	-14	123	1700	0.07	0	0	0	0.00	. 0	0	(0.00
1 N	3400	0.29 1	0	992	3400	0.29 ±	20	1012	3400	0.30 ±	-101	911	3400	0.27 ±	0	0	0	0.00	. 0	0	(0.00
	3800	0.18	-5		3800		15	703	3800		-70	633	3800	0.17	0	0	0	0.00	0	0	1	0.00
		0.11	0			0.11	0	186	1700	0.11	-19	167	1700	0.10	0	0	0	0.00	0	0	(0.00
		0.00		CLEARAN(CE	0.00		CLEXRXHO	Œ	0.00		CLEXRANC	E	0.00		CLEXRANC	CE	0.00		CLBARAN	CB	0.00
		==== 0.97		ICU VAL	JE	0.95		ICU VALU	JE .	0.98		ICU VALU	JE	0.89		ICU VAL	UE	0.00		ICU AYP	JE	0.00
R V	ERVIC	0.97		PRAEP O		0.95		TEAET OF		0.98					==== ALUE 0.89 OP SERVICE= D	ALUE 0.89	ALUE 0.89 ICU VAL	ALUE 0.89 ICU VALUE	ALUE 0.89 ICU VALUE 0.00	ALUE 0.89 ICU VALUE 0.00	ALUE 0.89 ICU VALUE 0.00 ICU VALU	ALUE 0.89 ICU VALUE 0.00 ICU VALUE

A:1420B1P.ICU

TABLE 2 A

VOLUME-CAPACITY ANALYSIS

ARCHIBALD AVENUE & WB SR-60 RAMPS

PM

	1995 C (Hayen/				1995 CON WITHOUT				PLUS PR TRA	OJECT PPIC			WITH 10 REDU	% TDM CTION									
ткакауок	AOPAR	CAP	V/C RATIO		TOTAL	CAP	V/C RATIO		TOTAL	CAP	V/C RATIO		TOTAL VOLUMB	CAP	V/C RATIO		TOTAL VOLUME	СЛР	V/C RATIO		TOTAL SMUJOV	CAP	V/C RATIO
NBL	331	1700	0.19 *	0	331	1700	0.19 *	0	331	1700	0.19 *	-33	298	1700	0.18 *	0	0		0.00	0	-	0	
NBT NBR	1242 0	5700 0	0.22 0.00	-15 0		5700 0	0.22 0.00	70 0	1297 0	5700 0	0.23 0.00	-130 0	1167 0	5700 0	0.20 0.00	0	-		0.00 0.00	0	-		0.00 0.00
SBL	0	0	0.00	0	0		0.00	0	0		0.00	0	0	0	****	0			0.00	0	-		0.00
SBT SBR	2699 812	5700 1700	0.47 0.48 *	-95 -60		5700 1700	0.46 *	110 65	2714 817	5700 1700	0.48 *	-271 -82	2443 735	5700 1700	0.43 ± 0.43	0			0.00 0.00	0			0.00 0.00
28L	0	0	0.00	0	0	0	0.00 ±	0	0	0	0.00 *	0	0		0.00 t	0	0	•	0.00	0	-	-	0.00
- EBT EBR	0		0.00 0.00	0	-	-	0.00 0.00	. 0	0		0.00	0	•		0.00 0.00	0	-		0.00	0			0.00
WBL	300	0	0.00	0	300		0.00	0	300		0.00	-30	270		0.00	0	-		0.00	0			0.00
WBT WBR	0 422	5700 0		0 -10	-	5700 0	0.12 * 0.00	0 40	0 452	5700 0	0.13 * 0.00	0 -45	•	5700 0	0.12 * 0.00	0			0.00	. 0	0		0.00 0.00
C	LEXRANCE		0.00		CPBYKYHO	E	0.00	(CLBARANC	E	0.00		CLEARANC	E	0.00		CLEARAN	CE	0.00		CLEARANC	!E	0.00
I	CU VALUE		0.80		ICU AYPſ	JE	0.77		ICU VALU	E	0.80		ICA AYP	JE	0.73		ICU AYPı	UE	0.00		ICU VALU	JE	0.00
L A:1420N2	EVEL OP P.ICU	SERVIC	E= C		PEAEP OE	' SBRV]	 CE= C		rsaer og	'SERVI	 [CB= C		LEVEL OF	SERV	 CE= C		PRAEP 01	P SERV	ICE=		PEAEP OF	' SERV	ICE=

TABLE <u>2 A .|</u>
VOLUME-CAPACITY ANALYSIS
ARCHIBALD AVENUE & WB SR-60 RAMPS
PM

	1995 C (Haven/	SR-60	Study)	***	1995 CON WITHOUT				PLUS PR TRA	OJECT FPIC			WITH 10 REDU	* TDM CTION									
KOYEKEN'	AOTAKE L	CAP	V/C RATIO		TOTAL	CAP	V/C RATIO		AOPAKE LOLYP	СХР	V/C RATIO		TOTAL VOLUME	CAP	V/C RATIO		TOTAL	CAP	V/C RATIO		TOTAL VOLUNE	СЛР	V/C RATIO
JBK TBK SBK	331 1242 0			0 -15 0	1227		0.10 * 0.22 0.00	0 70 0	1297	5700	0.10 ± 0.23 0.00	-33 -130 0	298 1167 0	3400 5700 0		0		0	0.00	0 0 0	0	0	0.00 0.00 0.00
SBL SBT SBR	0 2699 812	0 5700 1700	0.00 0.47 0.48 *	0 -95 -60	0 2604 752	0 5700 1700	0.00 0.46 * 0.44	0 110 65	2714	0 5700 1700	0.00 0.48 * 0.48	0 -271 -82	0 2443 735	5700	0.00 0.43 * 0.43	0 0 0	-	0	0.00 0.00 0.00	0 0 0	0	0	0.00 0.00 0.00
T EBL EBT EBR	0 0 0	0	0.00 0.00 0.00	0 0 0	0	0	0.00 * 0.00 0.00	0 0 0	0	0	0.00 ± 0.00 0.00	0 0 0	0	0	0.00 * 0.00 0.00	0 0 0	0	0	0.00 0.00 0.00	0 0 0	0	0	0.00
YBL YBT YBR	300 0 422		0.00 0.13 * 0.00	0 0 -10	0		0.00 0.12 * 0.00	0 0 40	0	-	0.00 0.13 * 0.00	-30 0 -45	0	5700	0.00 0.12 * 0.00	0 0 0	0	0	0.00 0.00 0.00	0 0 0	0	0	0.00 0.00 0.00
	CLEARANCE		0.00 ==== 0.71		CLEARANC		0.00 ==== 0.68		CLEARANC		0.00 ==== 0.71		ICU VALU		0.00 ==== 0.64		CLEARANC		0.00 ==== 0.00		CUEYLYNG		0.00 ==== 0.00
	LEVEL OP	SERVIO	:E= C		PEAEP OF	SERV	ICB= B		LEVEL OF	SERV.	ICE= C		reaer oi	? SERV	ICE= B		PEAEP OF	? SERV	ICB=		LEVEL O	F SERV	'ICE=

A:1420N2P.ICU

TABLE 28
VOLUME-CAPACITY ANALYSIS
ARCHIBALD AVENUE & WB SR-60 RAMPS
PM

		•	Study)				DITION PROJE			PLUS PR TRA	OJECT FPIC			WITH 10 REDU	* TDM CTION						~ ~ ~			
КОЛЕЖЕ	AOPAKE	CAP	V/C RATIO		. TOT.		CAP	V/C RATIO		TOTAL VOLUME	СЛР	V/C RATIO		TOTAL VOLUME	СЛР	V/C RATIO		TOTAL VOLUKE	CAP	V/C RATIO	۷OL.	TOTAL	СЛР	V/C RATIO
18К ТВК 8ВК		5700		-1	•	367 550 0	3400 5700 0	0.11 * 0.27 0.00	0 70 0	1620	5700	0.11 * 0.28 0.00	-37 -162 0	330 1458 0	3400 5700 0	0.10 * 0.26 0.00	0 0 0	0 0 0	0	0.00 0.00 0.00	0 0 0	0	0	0.00 0.00 0.00
SBI SBI SBI	3253			_		0 158 894	0 5700 1700	0.00 0.55 * 0.53	0 110 65	3268	0 5700 1700	0.00 0.57 * 0.56	0 -327 -96	2941	0 5700 1700	0.00 0.52 * 0.51	0 0 0	0	0	0.00 0.00 0.00	0 0 0	0	0	0.00 0.00 0.00
D 881 183 183	(0	0.00		0 0 0	0 0 0	0	0.00 * 0.00 0.00	0 0 0		0	0.00 [±] 0.00 0.00	0 0 0	0	0	0.00 * 0.00 0.00	0 0 0	0	0	0.00	0	0	0	0.00 0.00 0.00
%B1 %B1 %B1		5700	0.00 0.17 0.00		0	629 0 328	5700	0.00 0.17 ¹ 0.00	0 0 4 0	0	5700	0.00 0.17 * 0.00	-63 -37	0	5700	0.00 0.16 * 0.00	0 0 0	0	0	0.00	((_	0	0.00 0.00 0.00
	ICA AYP		0.00 ==== 0.85		ICA	RANC JJKV		0.00 ==== 0.83		CUBARAN		0.00 ==== 0.85		CUBARAN		0.00 ==== 0.78		CLEARANG		0.00 ==== 0.00		ICU VAL		0.00 ==== 0.00
A:142	LEVEL O				PEAE	3G 08	P SBRV	ICB= D		LEVEL O	P SERV	ICE= D		LEVEL 0	P SERV	ICE= C		PEAEP 0	P SERV	ICB=		PEAEP 0	P SERV	ICE=

TABLE 3 A

VOLUME-CAPACITY ANALYSIS

ARCHIBALD AVENUE & EB SR-60 RAMPS

PM

	1995 C (Baven/	SR-60	Study)		WITHOUT				PLUS PR TRA	OJECT FPIC			WITH 10 REDU	* TDM CTION							:		
колекен	T 8MUJOV	CAP	V/C RATIO		TATOT	CAP	V/C RATIO		TOTAL	СЛР	V/C RATIO		TOTAL VOLUME		V/C RATIO		TOTAL VOLUNB	CAP	V/C RATIO		TOTAL VOLUME	СУБ	V/C RATIO
NBC	0	0	0.00	0	0	0	0.00	0	0	0	0.00	0	0	0	0.00	0	0	0	0.00		0	C	0.00
NBT	1241	5700	0.25 *	-5	1236	5700	0.25 *	30	1266	5700	0.26 ±	-127	1139	5700	0.23 *	0	0		0.00	0			0.00
NBR	190		0.00	0		0	0.00	0	190	0	0.00	-19	171	0	0.00	(0	0	0.00	0	0	0	0.00
SBL	1030	3400	0.30 *	-60	970	3400	0.29 ±	65	1035	3400	0.30 ±	-104	931	3400	0.27 *	() 0	0	0.00	0	0	C	0.00
SBT	1969	5700		-35	,	5700	0.34	45		5700	0.35	-198	1781	5700	0.31	() 0	0	0.00	0	0	(0.00
SBR	0		0.00	0			0.00	0			0.00	0	0	0	0.00	() 0	0	0.00	0	0	0	0.00
J ERI.	332	٥	0.00	-10	322	٥	0.00	40	362	0	0.00	-36	326	0	0.00	() 0	0	0.00	0	0	(0.00
		-	0.13 *	•			0.13 *	0			0.14			5700	0.13 *	() 0	0	0.00	0	0	(0.00
EBT EBR	0 437		0.00	0			0.00	0			0.00	- 4 4	393	0	0.00	. (0 0	0	0.00	0	0	(0.00
	^	0	A AA +	0	0	n	0.00 *	0	0	n	0.00	. 0	0	0	0.00 ±	() 0	0	0.00	0	0	(0.00
XBL	0		0.00 *	0			0.00	0	-	-	0.00	0	-				0 0	0	0.00	0	0	1	0.00
¥BT ¥BR	0		0.00	0	•		0.00	0	•		0.00	0	=	-	0.00		0 0	0	0.00	0	0	(0.00
	CLDIDINC	D.	0.00		CLEARANO	۹-	0.00		CLEARAN	C.E.	0.00		CLEARAN	CE	0.00		CLEARAN	CE	0.00		CLEARAN	CE	0.00
	CLEXRANC	C	====		CDDVVVII	<i>.</i> u	====		O B B II II II II	0.5	====				====				====				====
	ICU AYPA	3	0.68		ICU VAL	UB	0.67		ICU VAL	UE	0.70		ICA AYP	UE	0.63		ICA AYP	UE	0.00		ICA AYP	UE	0.00
A:14201	LEVEL OF	SERVI	CE= B		PEAEP OI	P SBRV	ICE= B		LEVEL O	P SERV	ICE= B		PEAEP 0	F SERV	ICB= B		PBABP 0	F SBRV			PBABP 0	P SER'	

TABLE 38 VOLUME-CAPACITY ANALYSIS ARCHIBALD AVENUE & EB SR-60 RAMPS PM

	2010 ((Hayen/	'SR-60			2010 CO	T PROJE	CT		PLUS PR TRA				WITH 10 REDU	* TDM CTION						. 			
кочекен	T	CAP	V/C RATIO		. TOTAL	CAP	V/C RATIO		TOTAL	CAP	V/C RATIO		AOTAP AOTAP	СУБ	V/C RATIO		TOTAL VOLUKE	CAP	V/C RATIO		TOTAL VOLUME	CAP	V/C RATIO
NBC	0		0.00		0 (-	• • • •	0 30	0 1417	0 5700	0.00 0.29 *	0 -142	0 1275	0 5700	0.00 0.26 *	0		0	0.00	0		-	0.00
NBT NBR	1392 248	5700 0	0.29	x -	5 · 1387 0 248		0.29	0		• . • .	0.00	-25			0.00	0			0.00	0	0	C	0.00
SBL	1298	3400	0.38	i -{	0 1238		0.36 *	65	1303		0.38 ±	-130		3400	0.35 *				0.00	0			0.00
SBT SBR	2293 0		0.40	-(0 (0.40	45 0	2303		0.40	-230 0			0.36 0.00	(0.00	0			0.00
Jas C	439	0	0.00	-1	10 42) 0	0.00	40	469		0.00	-47	422		0.00	(0.00	0			0.00
EBT	0	5700	0.16	İ	0 48		0.16 *	0			0.17 ± 0.00	0 - 4 9			0.15 [*] 0.00	(0.00 0.00	0			0.00
XBC			0.00	i	0) 0	0.00 ±	0	0	0	0.00 1	0	0	0	0.00	: (0 0	0	0.00	0			0.00
YST	0	0	0.00		0	0 0	0.00	0	-		0.00	0	· ·		0.00 0.00		0 0 0 0		0.00	0			0.00 0.00
WBR	CLBARANC		0.00		CLEXRX		0.00		CLEARAN	CE	0.00		CLBYKYN	CE	0.00		CLEXRAN	CE	0.00		CLEARAN	CE	0.00
			0.83		ICU VA		0.81		ICU VXL	UE	0.84		ICA AYP	UE	0.76		ICU VAL	UB	0.00		ICU VAL	UE	0.00
	PEAEP OF						 ICE= D		PEAEP 0				[578] O	F SERV	 ICB= C		LEVEL O	P SER	 /ICE=		PBABP 0	P SER	VICE=

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A:1420B3P.ICU

TABLE 4A

VOLUME-CAPACITY ANALYSIS
PHILADELPHIA STREET & PROFORMA STREET
PM

	1995 C	ONDITI UT PRO			1995 CON WITH P				WITH 10 REDU														
KOAEKEN,	AOPAKE	CYB	V/C RATIO		TOTAL VOLUNE	CAP	V/C RATIO		TOTAL VOLUME	CAP	V/C RATIO		TOTAL	CAP	V/C RATIO		TOTAL VOLUMB	СЛР	V/C RATIO	VOL.	TOTAL VOLUMB		V/C RATIO
NBL NBT NBR	0	0	0.00 0.00 * 0.00	20 0 65	0		0.05 0.05 ± 0.00	-2 0 -6	0		0.05 0.05 * 0.00	0 0 0	0 0 0	0	0.00 0.00 0.00	0 0 0	0 0 0	0	0.00	0 0 0	0	0	0.00 0.00 0.00
SBL SBT SBR		1700 1900 0		0		1700 1900 0		-15 0 -4	0	1700 1900 0		0 0 0	0	0	0.00 0.00 0.00	0 0 0	0	0	0.00 0.00 0.00	0 0 0	0	0	0.00 0.00 0.00
DBBL CBBT CBBR	15 345 0	3800	0.05 ± 0.09 0.00	0 3 0 5	375	3800	0.05 ^x 0.10 0.00	-2 -38 -1	337	3800	0.05 [*] 0.09 0.00	0 0 0	0	0	0.00 0.00 0.00	0 0 0		0	0.00	0 0 0	0	0	0.00 0.00 0.00
WBL WBT WBR	-0 877 35	3800	0.00 0.24 *	10 30		3800	0.25 1	-1 -91 -4	816			0 0 0	0	0	0.00 0.00 0.00	0 0 0		0	0.00 0.00 0.00	•	0 0	(0.00 0.00 0.00
	CLBARANC		0.00 ==== 0.38		CLEARAN ICU VAL		0.00 ==== 0.44		CLEYLYH	•	0.00 ==== 0.40		ICU AYP		0.00 ==== 0.00		ICU VAI		0.00 ==== 0.00		ICU VAL		0.00 ==== 0.00
	LEVEL OF		 CB= λ		PEAEP 0	F SBRV	ICB= y		PEAEP 0	P SERV	ICB= X		LEVEL O	e serv	ICE=		PEAEP (P SER			TBASP 0	F SER	VICE=

A:1420N4P.ICU

TABLE 48

VOLUME-CAPACITY ANALYSIS
PHILADELPHIA STREET & PROFORMA STREET
PM

		2010 C			***************************************	WITH P				WITH 109															
ĸc	ткакау	AOLAKE	CAP	V/C RATIO	VOL.	TOTAL		V/C RATIO		SKUJOV Skujov	CAP	V/C RATIO		TOTAL VOLUME	C A P	V/C RATIO		TOTAL	CAP	V/C RATIO		TOTAL VOLUME	CAP	۷ / R A 1	
	NBL NBT NBR	0 0	0	0.00 0.00	20	20	1700 1900	0.05 0.05 * 0.00	-2 0 -6	0	1900	0.05 0.05 * 0.00	0 0 0	0	0	0.00 0.00 0.00	. (0 0	0	0.00 0.00 0.00	0 0 0	0	(0.0	00
	SBL SBT SBR	150 0 45		0.09 0.05 0.00	(0.09 * 0.05 0.00	-15 0 -4	0	1900	0.08 * 0.05 0.00	0 0	0	0	0.00 0.00 0.00		0 0 0 0 0 0	0	0.00 0.00 0.00	. 0	0	(0 0. 0 0. 0 0.	00
2	ebl ebt ebr		3800	0.05 0.14 0.00	3(0 15 0 544 5 5	3800	0.05 * 0.14 0.00	-2 -54 -1	490	3800	0.05 0.13 0.00	* 0 0	0	0	0.00 0.00 0.00		0 , 0 0 0 0 0	0	0.00	0	0	1	0 0. 0 0. 0 0.	00
	WBL WBT WBR	0 1069 35	0 3800	0.00 0.29 0.00	11 2 3	0 10	1700 3800	0.05 0.30 *	-1 -110 -4	989	1700 3800 0		t (0 0	0	0.00 0.00 0.00		0 0 0 0	0	0.00	(() 0)	0 0. 0 0. 0 0.	.00
		CLBARANC		0.00		CLBARAN		0.00 ==== 0.49		CLEARANC		0.00 ==== 0.45		CLEARANO		0.00 ==== 0.00		CCBYLYR		0.00 ==== 0.00		CLBARAN		== 0.	.00 === .00
		LEVEL OF				PBASP 0		 ΙCΒ= λ		PEAEP O	P SERV	 ΙCΕ= λ		PEAEP O	P SERV	 ICB=		PEASP (P SER	VICE=		CBABC ()F SER		=

λ:1420B4P.ICU

12-1986

Figure 9-1D

TRAFFIC SIGNAL WARRANTS

Philadelphia/Proforma-Project Driveway

(Based on Estimated Average Daily Traffic - See Note 2)

Near-Term 1995 Volumes

	.RURAL			um Requirements EADT				
1. Minimum Vehicular								
Satisfied	Not Satisfied X	Vehicles per street (total c approaches)	•	Vehicles pe volume mir (one direct	or-street a	- 1		
Number of lanes for moving to	raffic on each approach	<u> </u>	717		<u>r</u>	_ - -		
Major Street	Minor Street	Urban	adelphia Rural	Urban Pra	forma Rural	Project		
1	1	8,000	5,600	2,400	1,680	7.7		
2 or more	1	9,600	6,720	2,400	1,680			
	2 or more	9,600 13,47	0 6,720	3,200 1,9	50 2,240	800		
1	2 or more	8,000	5,600	3,200	2,240			
2. Interruption of Continuous	Traffic							
Satisfied	Not Satisfied X	Vehicles per street (total of approaches)	of both	Vehicles per day on higher- volume minor-street approac (one direction only)				
Number of lanes for moving t	raffic on each approach					,		
I		PLil	hdulphia	Pa	Rural	Project		
Major Street	Minor Street	Urban	Rural	Urban		Dwy		
,	1	12,000		1,200				
	1	14,400	10,080	1,200	850			
2 or more	2 or more	14,400 13,4	17010,080	1 ''	50 1,120	800		
1	2 or more	12,000	8,400	1,600	1,120			
3. Combination								
Satisfied	Not Satisfied							
	out following warrants fulfilled	2 W	Varrants	2	Warrants			
80% or more	***************************************							
	1 2							

NOTE:

- 1. Heavier left turn movement from the major street may be included with minor street volume if a separate signal phase is to be provided for the left-turn movement.
- 2. To be used only for NEW INTERSECTIONS or other locations where actual traffic volumes cannot be counted.
- 1-Based on expansion of PM peak hour volumes (see Exhibit 6), assuming 10% of the daily volume occurs during the PM peak hour.

Calculation of Gaps in Southbound Traffic Stream on Archibald at Project Driveway

EBR @ Phil/Archibald = 142 vph

For a 100 sec cycle there is 36 cycles/hour

... veh/cycle = 142/36 = 3.94

EBR Saturation Flow = 1700 vph

= 1700 = 0.47 veh/sec or 2.12 sec/vehicle

Time to clear EBR = 3.94 veh/cycle x 2.12 sec/veh = 8.35 sec/cycle Add 2 sec. lost time

Total Gap available for NBL at Project Driveway (based on Passer II run)

= NBL @ Phil. + E/W @ Phil. - EBR @ Phil.

= 10 + 20 - 11.0 = 19 sec

NBL @ Project Driveway = 100 vph
= 2.78 veh/cycle based on 100 sec cycle
peak volume per cycle = 1.5 x 2.78 = 4.17 veh/cycle

available gap per vehicle = 19 sec/cycle 4.17 vel/cycle

= 4.56 sec/vehicle

4.56 sec/veh is adequate to clear vehicles

TEXAS DEPARTMENT OF HIGHWAYS AND FUBLIC TRANSPORTATION MULTIPHASE ARTERIAL PROGRESSION - 145101 3.0 JULY 1986 PASSER2 PASSER II-84

ONTARIO

ARCHIBALD AVE DISTRICT 12 07/02/90 RUN NO. 1

OPTIONS IN EFFECT ARE:

PROGRESSION MODE. DIRECTIONAL ORIENTATION SPECIFIED (NARROW FORMAT ONLY).

ARTERIAL ORIENTATION (A-DIRECTION) IS: SB.

NARROW (SCREEN) OUTPUT FORMAT.

GRAPHIC DISPLAY FILE OUTPUT TO UNIT 9.

NUMBER OF INTERSECTIONS LENGTH

LOWER CYCLE

UPPER CYCLE LENGTH

CYCLE INCREMENT

1.00

100

5

** INTERSECTION 1 PHILADELPHIA

O. FT SPEED O. MPH

DISTANCE 1 TO 0

SPEED

O. FT

O. MPH

O SECS

A SIDE QUEUE CLEARANCE B SIDE QUEUE CLEARANCE

O SECS

ARTERIAL PERMISSIBLE PHASE SEQUENCE.

LEFT TURNS FIRST

THROUGH MOVEMENTS FIRST WITH OVERLAP

LEADING GREEN

LAGGING GREEN

WITH OVERLAP

WITH OVERLAP WITH OVERLAP

CROSS ST FHASE SEQUENCE IS LEFT TURNS FIRST

WITH OVERLAR.

				1410	OVEMENTS	(NEM	4)		
		5	ેં	1.	22	3	4	7	8
VOLUMES (VPH) SAT FLOW RATE	(VPHG)	143 3400	1329 5100	18 3400	3018 5100	446 3400	703 3400	1012 3400	361 3400
MINIMUM GREEN	(SEC)	1. ()	25	1. O	2.5	1. ()	20	1. O	20

TEXAS DEPARTMENT OF HIGHWAYS AND FUBLIC TRANSFORTATION MULTIPHASE ARTERIAL PROGRESSION - 145101 3.0 JULY 1986 PASSER II-84

INTERSECTION 2 WB SR-60 RAM

DISTANCE 1 TO 2 SPEED DISTANCE 2 TO 1 SPEED 910. FT 40. MPH 910. FT 40. MP

40. MPH

A SIDE QUEUE CLEARANCE

A SIDE QUEUE CLEARANCE O SECS

O SECS

ARTERIAL PERMISSIBLE PHASE SEQUENCE.

THROUGH MOVEMENTS FIRST WITH OVERLAP

CROSS ST PHASE SEQUENCE IS THROUGH MOVEMENTS FIRST WITH OVERLAP.

			141	OVEMENTS	(MEMA	١)		
	Ü	ර	:1.	2	3	4	7	83
VOLUMES (VPH)	()	1620	367	3268	0	997	()	()
SAT FLOW RATE (VPHG)	O	5100	3400	5100	()	5100	$\langle \rangle$	O
MINIMUM GREEN (SEC)	\Diamond	1.0	1.0	1. ()	0	30	()	0

**** INTERSECTION 3 EB SR-60 RAM

DISTANCE 2 TO 3 SPEED 475. FT

40. MPH

DISTANCE 3 TO 2 SPEED: 475. FT

40. MPH

A SIDE QUEUE CLEARANCE B SIDE QUEUE CLEARANCE

O SECS

O SECS

ARTERIAL PERMISSIBLE PHASE SEQUENCE.

THROUGH MOVEMENTS FIRST

WITH OVERLAR

CROSS ST PHASE SEQUENCE IS THROUGH MOVEMENTS FIRST WITH OVERLAP.

			MC	VEMENTS	(MEMA)			
	5	ර	1.	2	3	4	7	8
VOLUMES (VPH)	1303	1665	()	2303	()	0	O	956
SAT FLOW RATE (VPHG)	3400	5100	()	5100	()	O	()	5100
MINIMUM GREEN (SEC)	1.0	1.5	0	1.5	\Diamond	()	\Diamond	30

PASSER2

🧦 k INTERSECTION 1 PHILADELPHIA OFFSET= .0 SECONDS, .0 %

ARTERIAL PHASE SEQUENCE IS LEADING GREEN CROSS STREET PHASE SEQUENCE IS LEFT TURNS FIRST

		ARTER	II.AL		CRO)SS ST	REET	
MOVEMENTS .	2+5	2+6	148	TOTAL.	347	4+7	448	TOTAL.
GREEN TIME (SECS)	10.2	328	10.0	53.0	19.1	7.9	20.0	47.0
GEREN TIME (%)	10.2	32.8	10.0	53.0	19.1	7.9	20.0	47.0

	EMENT		RA" (卷)	/C TIO (LOS)	TOTAL (VEH-HR)	DELAY AVERY (SEC/VEH	(LOS)	PROB. OF QUEUE CLEAR.(%)	STOPS (VEHZHR)(%)	DELAY DELAY
NB	THRU		67	(B)	9.80	26.5	(C)	1.00	1010. (76)	
	L_E_F_T	1	9	(A)	.22	44.4	(D)	1.00	16. (86)	
SB	THRU	Ħ	152*	(F)	492.62	587.6	(F")	()	4076. (135)	
	LEFT	¥	68	(E)	2,12	53.4	(E)	84	128. (89)	
EB	THRU	5	66	(B)	4,23	42.2	(D)	96	308. (85)	
	LEFT	## FT	87	(E)	6.81	54.9	(⊞)	59	396. (89)	
WB	THRU	ä	87	(E)	8.86	45.4	(D)	69	611. (87)	
	L.E.F.T.	=	129*	(F')	78.63	279.7	(F)	0	1006. (99)	
FIGDE	E 1.	::	1.52*	(MAX)	603.29	308.9			7550. (107)	120

**** INTERSECTION 2 WB SR-60 RAM OFFSET= 4.5 SECONDS, 4.5 %

ARTERIAL PHASE SEQUENCE IS THROUGH MOVEMENTS FIRST CROSS STREET PHASE SEQUENCE IS THROUGH MOVEMENTS FIRST

NODE 2 : 126*(MAX) 185.51 106.8

		REET	DSS STE	CRO		CAL.	ARTER						
	TOTAL	3+7	348	4+8	TOTAL	1.4.5	1.46	2+6			3	EMEINTE	MOVE
	30.0	. ()	()	30.0	70.0	" ()	12.6	57.4	3)	(SECS	1E	H TIP	GREE
	30.0	()	O	30.0	70.0	. O	12.6	57.4		(光)	IIE.	H TIP	GREE
MIN			COEC.	to do		ELAY	DI		/C	V,			
DELAY	OF:S	ST	MEDE	Otal G	RAGE	AVE	TAL.	π.Ο	r II O	RA"		THENT	MOVE
CYCLE	HR)(%)	(VEHZ		1)(LOS)	SEC/VEI		(VEH	(LOS)	(%)				
	(1.1.)	174.)()	3. <	(A)	2.1	.95		(A)	48	## ##	THRU	NB
	(93)	343.	()		(F)	266.9	.21	27	(F)	1,26*	\$00 84	LEFT	
	(98)	3198.	()		(F")	162.3	.31	1.47	(F)	120*	91	THRU	SE
	(83)	830.	26	9	(I))	36.3	.05	1.0	(C)	75	16 F1	THRU	WE

4545. (73) 120

TEXAS DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION MULTIPHASE ARTERIAL PROGRESSION - 145101 3.0 JULY 1986 PASSER2 PASSER II-84

788. (82)

3947. (63) 120

120

EB THRU : 72 (C)

LIATOT

NODE 3 : 115*(MAX) 123.45

: 19509.

INTERSECTION 3 ER SR-60 RAM OFFSET= 12.9 SECONDS, 12.9 %

98

811.5

ARTERIAL PHASE SEQUENCE IS THROUGH MOVEMENTS FIRST CROSS STREET PHASE SEQUENCE IS THROUGH MOVEMENTS FIRST

9..42

		ARTERIAL			CROSS STREET		
MOVEMENTS	•	2+6 2+	5 145 -	TOTAL.	4+8 3+	8 3+7 TOTAL	
GREEN TIME	(SECS)	32.6 37.	4 ()	20.0	30.0	0 .0 30.0	
GREEN TIME	(%)	32.6 37.	4 "0	70.0	300	0 .0 30.0	
	VZC		DELAY		PROB.		MIIN
MOVEMENT	RATIO	TOTAL	AVE	RAGE	OF QUEU	E STOPS	DELLAY
	(%) (LOS)	(VEH-HR)	(SECZVEI	H)(LOS)	CLEAR.(%) (VEHZHR)(%)	CYCLE
NB THRU :	115* (F)	62.52	135.2	(F)	0	1600. (96)	
SB THRU :	69 (B)	1.81	28	(百)	1.00	285. (12)	
LEFT :	115米 (円)	49.69	137.3	(F)	O	1274. (98)	

35.5

71.4

(D)

*** PASSER II-84 BEST SOLUTION SUMMARY - TOTAL SYSTEM PERFORMANCE ***

CYCLE LENGTH # 100

BAND WIDTH (SE SPEED (MP	CS)	A 32 40	B 16 40		EFFICIENCY ATTAINABILITY	: ::	.24 .65
PERFORMANCE	TOTAL	TOTAL.	AVERAGE	TOTAL	FUEL.	MAX	
MEASURES	VEHICLES	DELAY	DELAY	STOPS	CONSUMPTION	CYC	

(VEHZHR) (VEHZHR) (SECZVEH) (VEHZHR)(%) (GALZHR) (SEC)

912.2 168.3 16041.7(82)

TEXAS DEPARTMENT OF HIGHWAYS AND PUBLIC TRANSPORTATION

MULTIPHASE ARTERIAL PROGRESSION - 145101 3.0 JULY 1986 PASSER2 PASSER II-84

ARCHIBALD AVE -SPACE DIAGRAM FOR: RUN NUMBER 1 07/02/90 CYCLE LENGTH 100 ONTARIO DISTRICT 12 EB SR-60 RAM 12.98 12.9% * Ж: * WB SR-60 RAM 4.58 4.5% Ж *: ****Main Project Driveway ж *ж ж * PHILADELPHIA "B" BAND "A" BAND 40 MPH 40 MEH 16 SECONDS 32 SECONDS

SCALES: HORIZONTAL - 1 INCH = 20 SECONDS (1 INCH = 10 CHARACTERS)

*** BOTH LEFTS

==== BOTH THRUS

KEY:

(1+5) +++ LEADING GREEN (2+6) --- LAGGING GREEN

(2+5)

(1+6)

APPENDIX C

Police Security Standards

I. SECURITY LIGHTING

- A. All buildings are required to have minimal exterior lighting to eliminate any dark areas (to include any recessed areas). direct lighting shall be provided at all entrance ways.
- B. The <u>minimum maintained</u> lighting level shall be one (1) to one and one half (1 1/2) foot candle power in all parking, loading, common and storage areas.
- C. All areas are to be lighted from sunset to sunrise and will be controlled by photo sensored cells.
- D. Lighting in exterior areas shall be in vandal-resistant fixtures.
- E. The developer shall have submitted certified exterior site lighting plans showing luminaire throw patterns cut sheets of the luminaires. The lighting plans must be approved prior to building permits being issued.
- F. Lighting around the development is to be consistent.
- G. Interior night lighting shall be constructed and maintained on the ground floor level in those areas that are visible form the street.

II. SECURITY HARDWARE

- A. One (1) inch single cylinder. If windows are within forty (40) inches of any locking device, tempered glass must be used.
- B. Glass panel, aluminum frame swinging doors shall have astragal plate to protect the strike. Placement must conform with Fire Department standards.
- C. Sliding glass doors will be of the inside sliding door type. Track mounted locking slidebolts and anti-lift devices will be installed on all sliding glass doors.

- D. Large garage-type/loading doors are to have two slide bolts, one on each side of the doors.
- E. All roof openings giving access to the buildings shall be secured with either iron bars, metal gates, stamped metal, or alarmed and meet with Police Department approval.
- F. All skylights shall be constructed of a "burglar resistant" material, or be secured with either iron bars or an alarm system, and meet with Police Department approval.

III. SECURITY FENCING

- A. No obstructing material will be used on any entrance gate.
- B. Block or chain link fencing will be a minimum of six (6) feet tall around storage areas.

IV. NUMBERING

- A. Street address numbering shall adhere to standards set forth in City of Ontario Ordinance 9-3.2746(3). Numbers and the background to which they are attached shall be of contrasting colors and shall be of a reflective material for nighttime visibility.
- B. The developer shall install roof top numbers and street names on all roofs of a development. They shall be a minimum of three (3) feet in length and two (2) feet in width and of white color. Numbers shall be placed parallel to street address as assigned.
- C. Buildings with rear access must have the numbers meeting the requirements of IV-A, above.

V. SECURITY SHRUBBERY

A. Security shrubbery shall be installed next to all fences and walls that adjoin all common/public access areas. Placement of such shrubbery will meet all requirements of the City of Ontario Development Advisory Board.

VI. ALARM SYSTEMS

- A. A burglar alarm system is recommended for all businesses, and a robbery alarm should be considered for certain retail businesses.
- B. If an alarm is installed, an alarm permit must be obtained from the Ontario Police Department. Subscribers should acquaint themselves with Ontario's False Alarm Ordinance, OMC 4-9.1990.
- C. If an alarm is installed, a blue flashing light shall be installed on the roof top, screened from public view but visible from the air.

VII. MISCELLANEOUS

- A. The developer shall provide a copy of these requirements to his or her on-site contractor.
- B. The placement of outside public telephones shall be restricted to an area immediately adjacent to the front door of the development.